

R&D activities on sCO₂ in Europe: Components Challenge – Heat Exchangers [1]

Recuperators and coolers

Third episode – 6 March 2023

This webinar is in cooperation with 8 European R&D projects

COMPAS_sCO₂

SCARABEUS 


CO₂OLHEAT


sCO₂-4-NPP

CARBOSOLA

sCO₂-Efekt

 DESOLINATION


SOLAR
sCO₂OL

Webinar content & speakers

- **Fundamentals, challenges and recent research** and development activity on sCO₂ cycle recuperators and coolers (Savvas Tassou – Brunel University of London)
- **Printed circuit heat exchangers** for sCO₂ power cycles (Natalie Sarpong & Daniel Georges – Heatric)
- **Improvement of dry air cooler for the condensation of blended CO₂ using enhanced tubes** (Xavier Guerif – Kelvion Thermal Solutions)



sCO₂ Recuperators and coolers

Challenges and recent research and development

Savvas Tassou and Lei Chai



savvas.tassou@brunel.ac.uk

Brunel University London

Research and Development on sCO₂ cycles and components

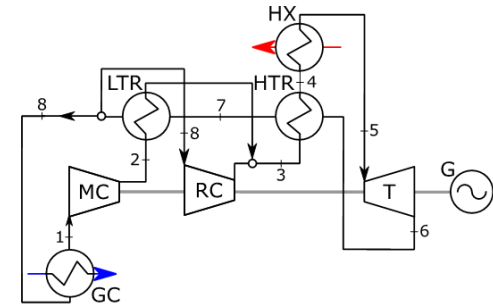
Institute of Energy Futures

- CO₂ refrigeration ; CO₂ high temperature heat pumps ; sCO₂ heat to power
- I-ThERM - (60 kWe simple recuperative cycle)
- CO₂OLHEAT – (2.0 MWe waste heat to power)
- SCOTWOHR – UKRI – Cycle optimisation for heat recovery and HXs

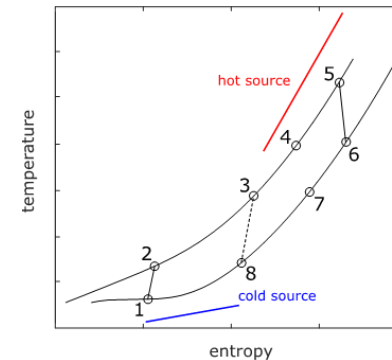


Heat exchangers in sCO₂ cycles

- Many sCO₂ cycle configurations possible for different applications
- Number of heat exchangers can vary
- Minimum 3 (heater, gas cooler and recuperator) in simple recuperated cycle.
- Multiple heat exchangers in complex cycles
- Heat exchangers responsible for significant capital cost in sCO₂ systems



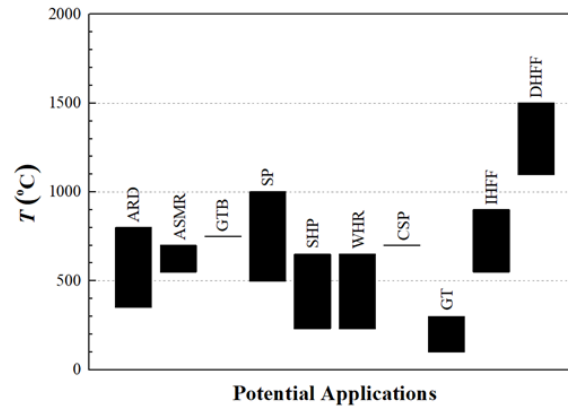
Recompression cycle



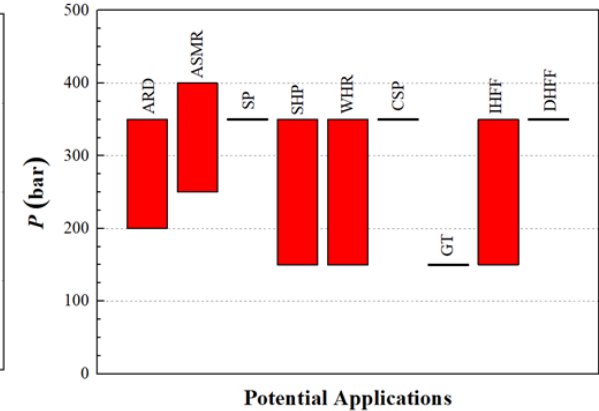
sCO₂ heat exchanger design considerations

Very favourable thermophysical properties of CO₂ in supercritical region can enable wide range of applications and operating conditions.

- Operation at high pressures and temperatures can lead to high cycle efficiencies.
- Implications on:
 - material selection
 - manufacturing methods
 - life cycle costs



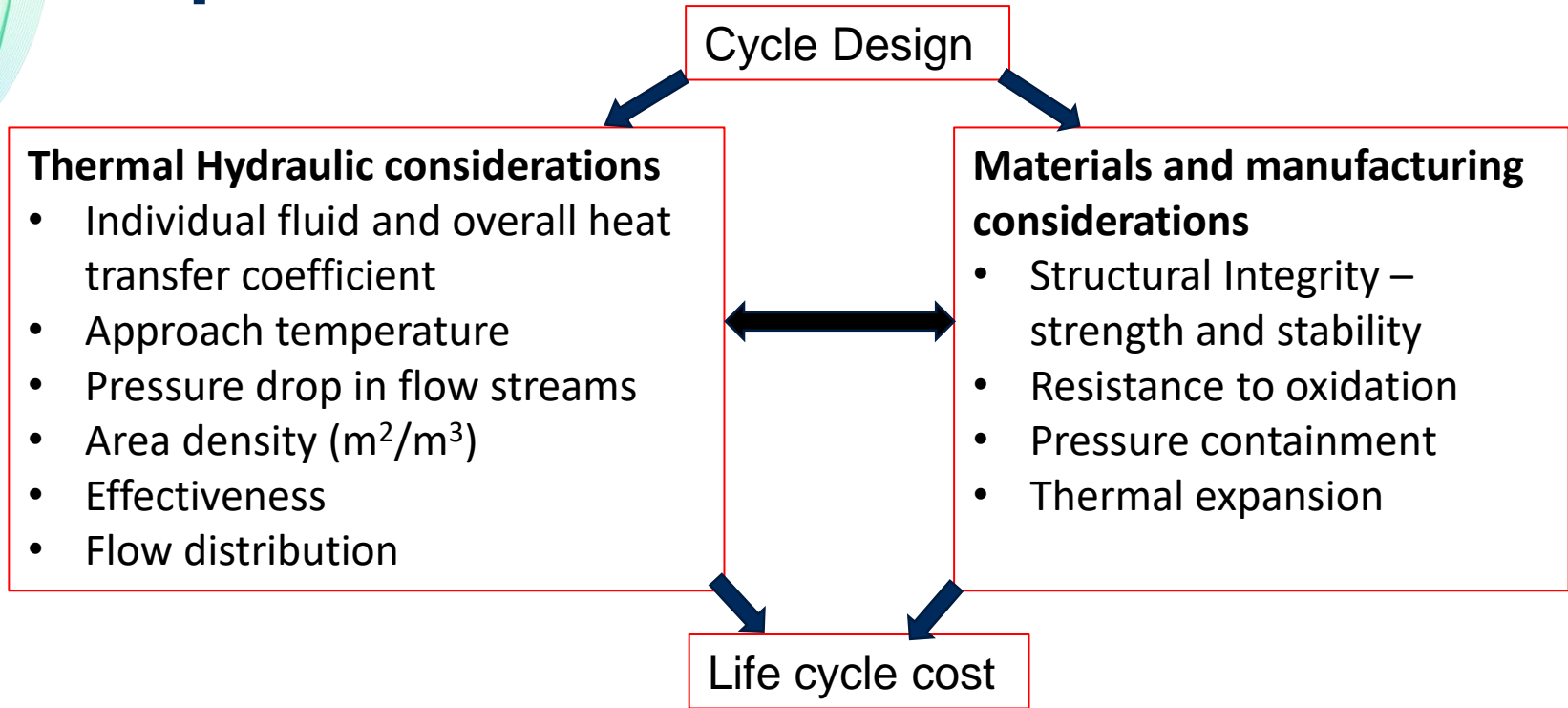
ARD (advanced reactor designs)
 ASMR (advanced small modular reactors),
 GTB (gas turbine bottoming),
 SP (shipboard propulsion),
 SHP (shipboard house power),



WHR (waste heat recovery),
 CSP (concentrated solar power),
 GT (geothermal),
 IHFF (indirect heating fossil fuel),
 DHFF (direct heating fossil fuel).

From: Mendez and Rochau, SAND-2018-6187, Sandia National Laboratories, Albuquerque, New Mexico, 2018.

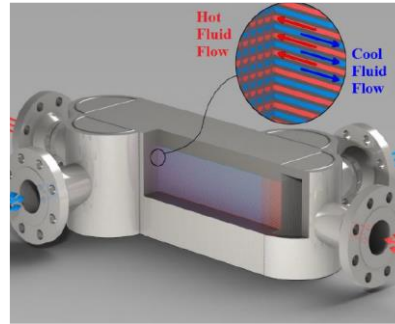
Challenges for heat exchangers/ recuperators and coolers



Heat exchanger types for recuperators

Recuperators (sCO₂ to sCO₂)

- Shell and tube
- Plate and shell
- Spiral wound exchanger
- Compact heat exchangers
 - Printed Circuit (PCHE)
 - Microtube heat exchangers
 - Plate matrix heat exchangers
 - Pin finned heat exchangers
 - Additively Manufactured HXs



PCHE

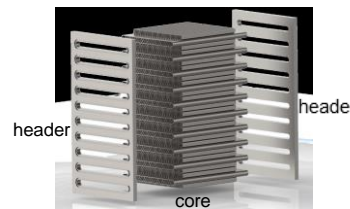
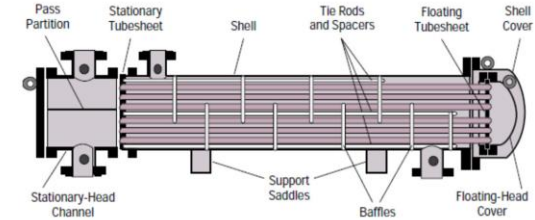


Plate-matrix HX

Musgrove et.al. 2018
CO₂ Power Cycles Symposium

Shell and tube



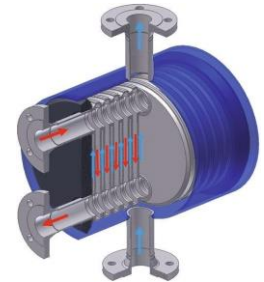
(<https://www.enggyclopedia.com/2019>)

Spirally wound



<http://www.wingtech.com/en>

Plate and shell



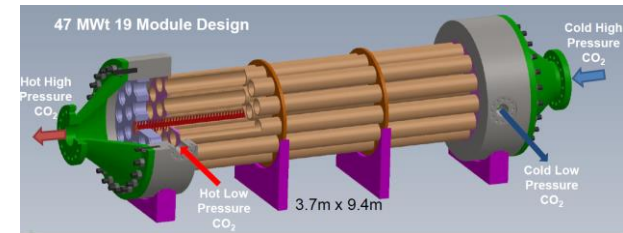
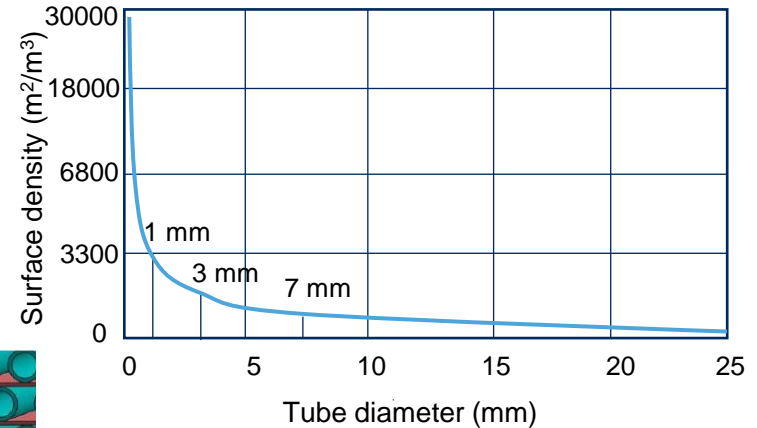
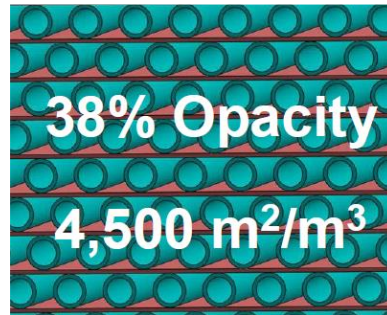
www.elevatedflaresystem.com/

Microtube heat exchangers

Can be used as primary heaters, recuperators and coolers

- Recuperators very similar to shell and tube
- Numerous tubes in bundles in a shell

Category	Units	#
Duty @ 20 kg/min sCO ₂	kW	150
Effectiveness	%	97.5
High Pressure Outlet T	°C	529
High Pressure Delta P	bar	< 0.1
Low Pressure Outlet T	°C	189
Low Pressure Delta P	bar	0.1
Length	m (ft)	2.78 (9.12)
Pipe Dia	m (ft)	0.23 (0.75)
Flange Dia	m (ft)	0.38 (1.25)



Prototype design of microtube HX for STEP project

Thar Energy, 2018 DE-FE0026273 project

Microtube heat exchangers – thermal-hydraulic modelling for optimisation

Modelling of compact heat exchangers for CO₂ ideally should apply the segmental approach due to large changes in fluid properties particularly close to the critical point.

$$U_i A_i = \frac{1}{\frac{1}{h_{c,i} A_{c,i}} + R_{s,i} + \frac{1}{h_{h,i} A_{h,i}}}$$

$$\varepsilon_i = \frac{1 - \exp[-NTU_i(1 - C_i^*)]}{1 - C_i^* \exp[-NTU_i(1 - C_i^*)]}$$

$$NTU_i = \frac{U_i A_i}{C_{\min,i}}$$

$$C_i^* = \frac{C_{\min,i}}{C_{\max,i}}$$

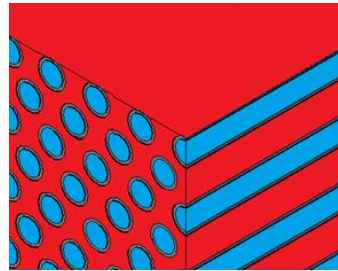
$$C_{\min,i} = \min(\dot{m}_{c,i} c_{pc,i}, \dot{m}_{h,i} c_{ph,i})$$

$$C_{\max,i} = \max(\dot{m}_{c,i} c_{pc,i}, \dot{m}_{h,i} c_{ph,i})$$

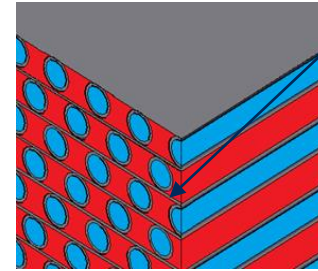
Gnielinski correlations

$$Nu_{c,i} = \frac{(f_{c,i}/8)(Re_{c,i} - 1000)Pr_{c,i}}{1 + 12.7(f_{c,i}/8)^{1/2}(Pr_{c,i}^{2/3} - 1)} \quad \text{Cold side}$$

$$Nu_{h,i} = \frac{(f_{h,i}/8)(Re_{h,i} - 1000)Pr_{h,i}}{1 + 12.7(f_{h,i}/8)^{1/2}(Pr_{h,i}^{2/3} - 1)} \quad \text{Hot side}$$

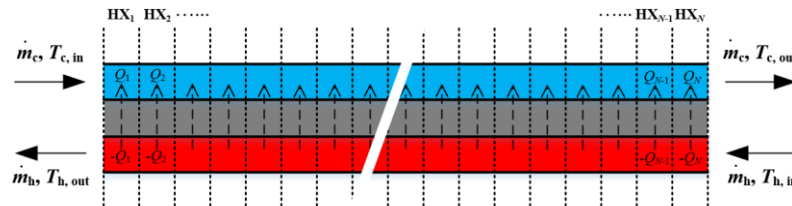


MTHE



MTHE-SS (separator sheets)

Separator sheets



Microtube heat exchangers

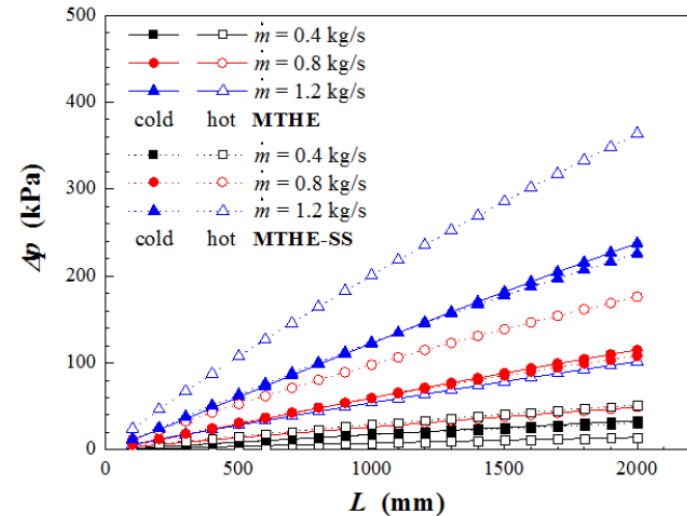
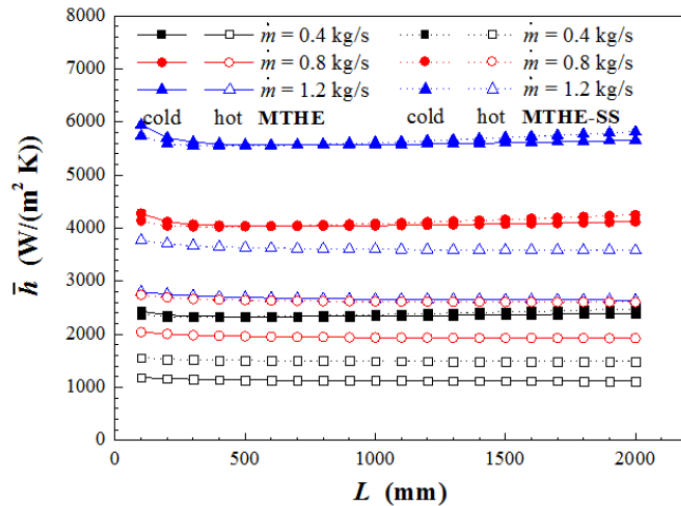
Comparison between tube bundles with and without separator sheets

Microtube with baffles – cross counter flow

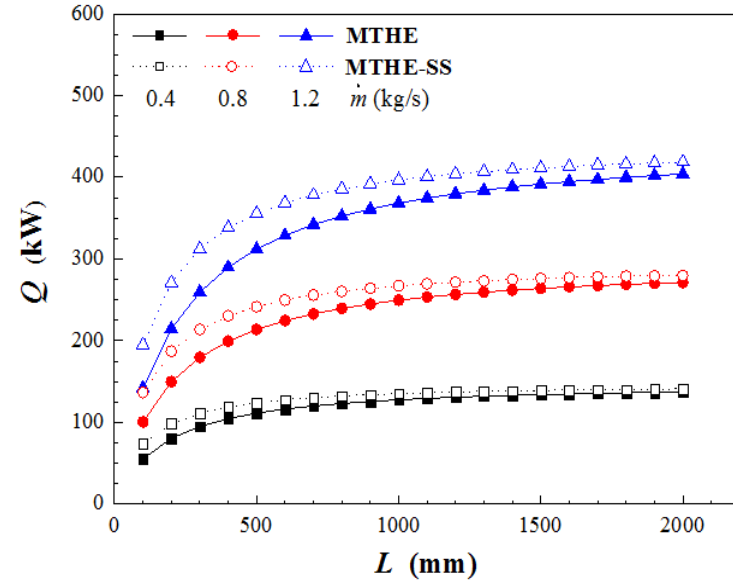
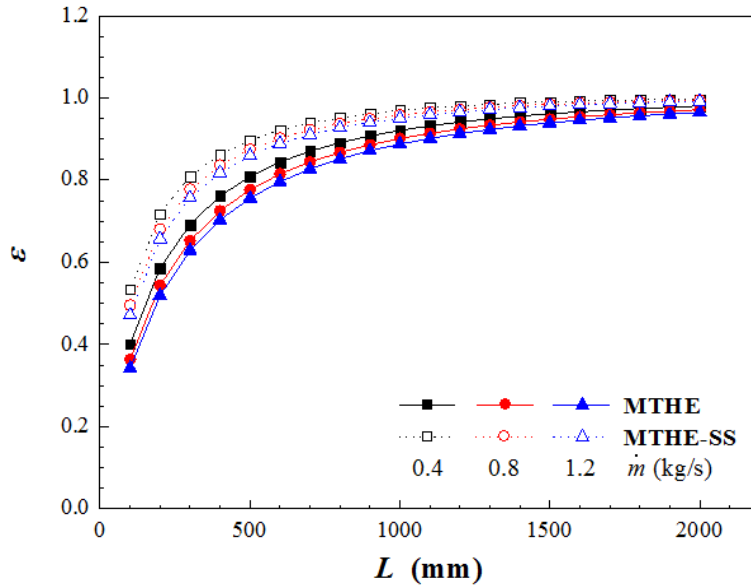
Tube diameter 1.0 mm; thickness 0.1 mm

Microtube with separator sheets counter current flow

$T_{c,in} = 100\text{ }^{\circ}\text{C}$, $T_{h,in} = 400\text{ }^{\circ}\text{C}$, $p_{c,in} = 150\text{ bar}$, $p_{h,in} = 75\text{ bar}$,

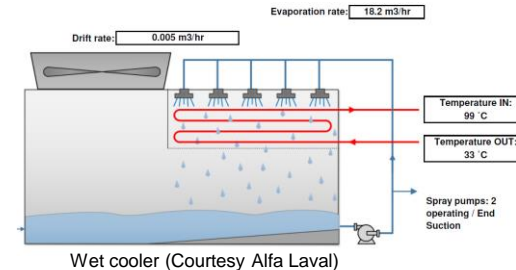
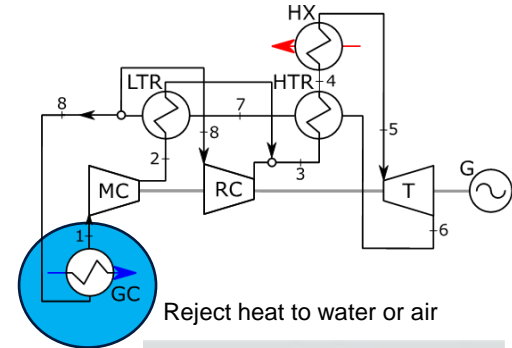


Microtube heat exchangers



Coolers

- Less demanding operating conditions than recuperators – (max. ambient temperature; pressure equalisation in power block; CO₂ management).
sCO₂ inlet 80-100 bar; 80-100 °C; CO₂ outlet 32-40 °C.
- Heat Exchangers
 - Rejection of heat to water
 - Shell and tube
 - Plate and shell
 - Compact heat exchangers
(important to be able to clean and repair tubes and flow passages-or filter/treat the water)
 - Rejection to air (CO₂ to air – direct cooling)
 - Finned tube heat exchangers (dry coolers)
 - Bare tube heat exchangers (wet coolers)
 - Adiabatic coolers
 - Microtube heat exchangers



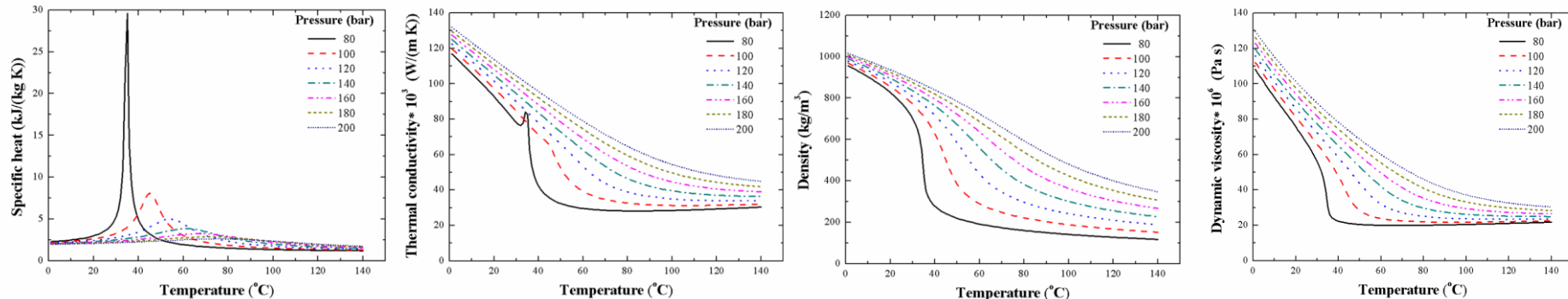
Summary

- PCHEs well established as recuperators
- Other emerging compact designs – it will take time before they are established commercially for multi-MWth applications.
- Selection of cooler type will depend on availability of water and ambient temperature.
- Heat transfer and pressure drop correlations based on modelling and testing on single tubes or small components-need to be validated on larger full size components
- Wet direct cooling may be a good lower life cycle cost option compared to indirect cooling – area of further research?

Back up slides

CO₂ working fluid in sCO₂ power cycles

- CO₂ is a dense working fluid with very good thermophysical properties
- Very compact heat transfer equipment compared to other heat transfer fluids used in power generation
- Low critical temperature, 31.1 °C; Critical pressure 73.8 bar
- Very good thermophysical properties particularly close to critical point



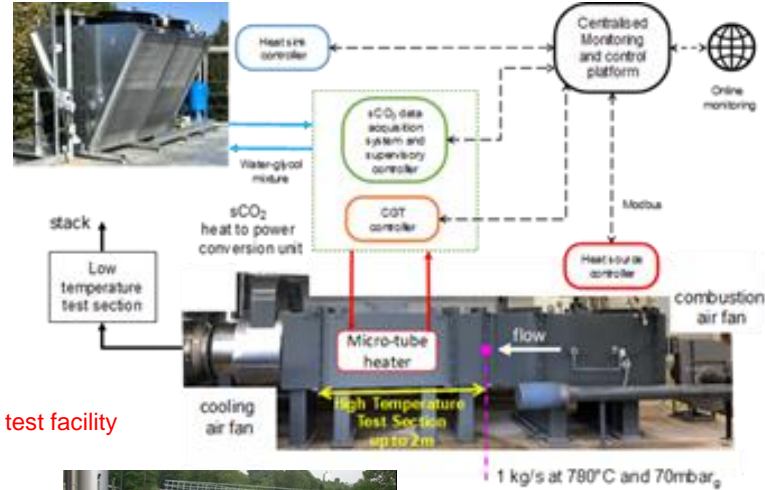
Thermophysical properties of CO₂ at different pressures versus temperature (constructed using Refprop)

Chai&Tassou *Journal of Enhanced Heat Transfer* 29(4):1–40 (2022)

Research and Development on sCO₂ cycles and components



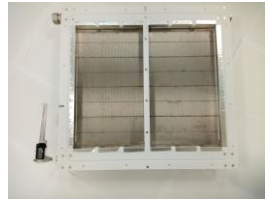
60 kWe sCO₂ power block



sCO₂ test facility



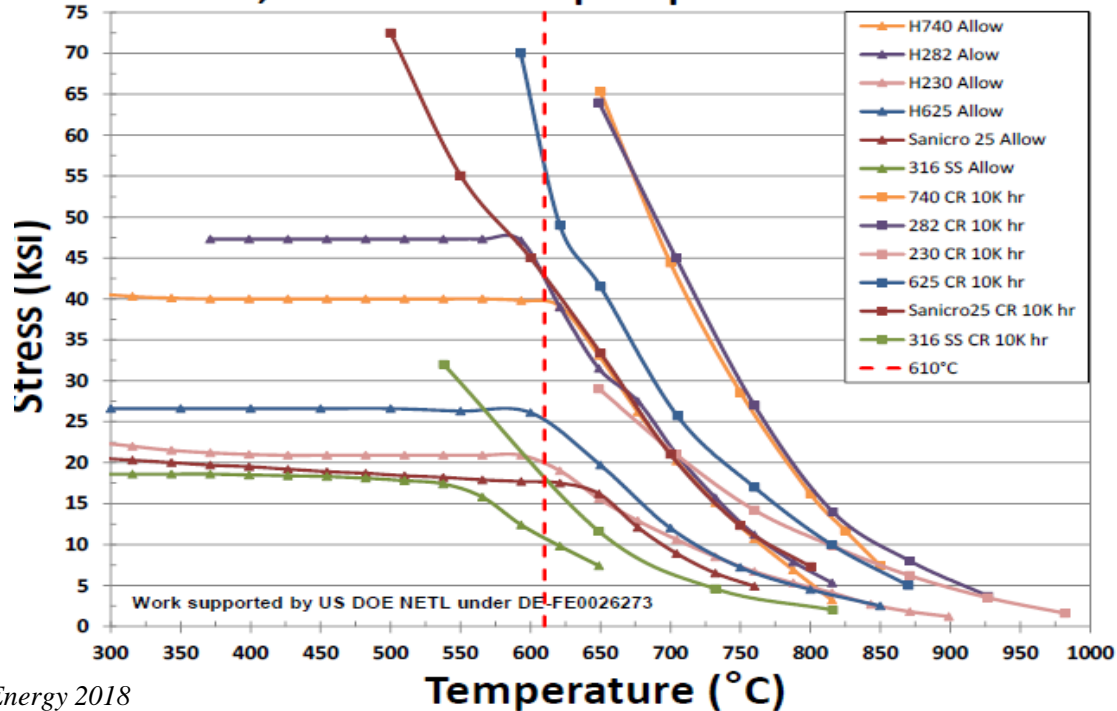
Microtube test facility



Gas cooler test facility

CO2 working fluid in sCO2 power cycles

ASME Allowable Stress and 10,000 Hour Creep Rupture Values



Courtesy – Thar Energy 2018

Printed circuit heat exchangers for sCO₂ power cycles

presented by Daniel Georges and Natalie Sarpong

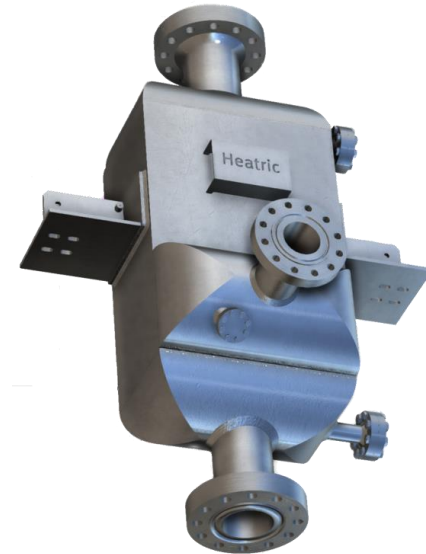
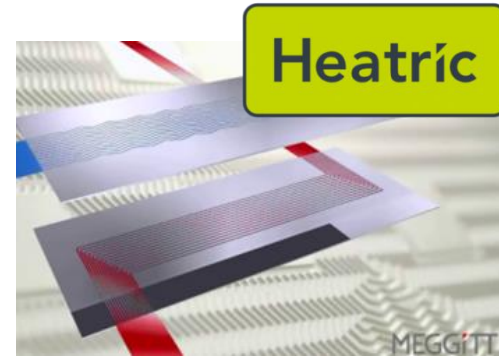
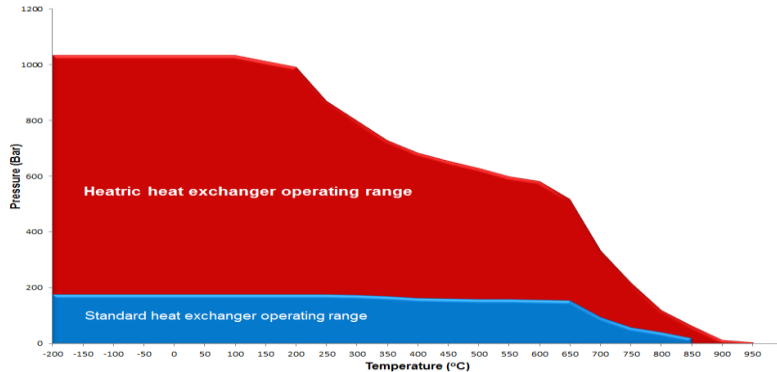


- What is a PCHE? 3
- PCHE uses in sCO₂ cycles 4
- Challenges 5-7
- Solutions 8
- Current Path to Commercialisation 9

What is a PCHE?

Printed Circuit Heat Exchanger

- Chemically etched plates
- Diffusion bonded core
- High temperature and pressure capability



PCHE uses in sCO₂ cycles

Recuperators and Coolers

- **Recuperators**
 - Recover heat from the hot side of the cycle to heat the cold side
 - Improves efficiency
- **Coolers**
 - Cools the cycle prior to re-entering the compressor
 - For closed loop cooling systems
- **Advantages**
 - Performance
 - Safety
 - Size
 - Cost

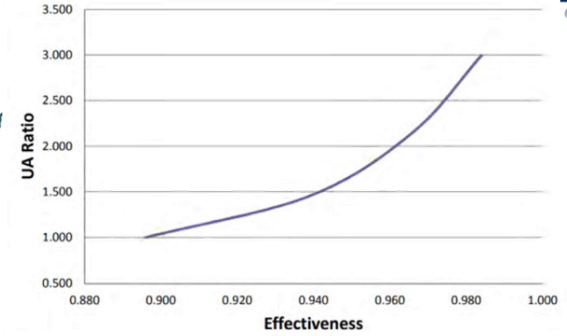
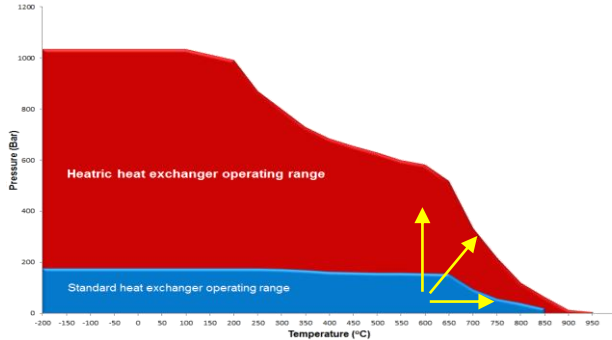
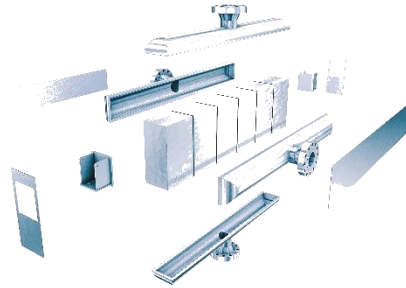
Heatric



Challenges

Design Conditions

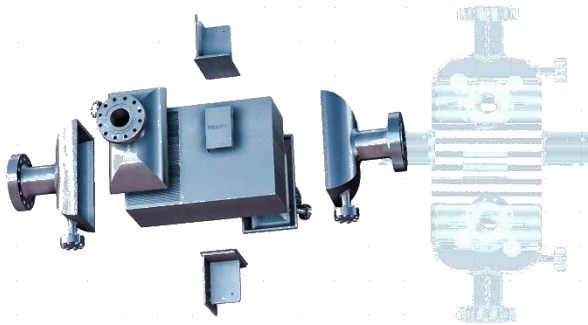
- Higher T/P Operation
- Larger Temperature Span
- Material selection based on DT_{max}



Challenges

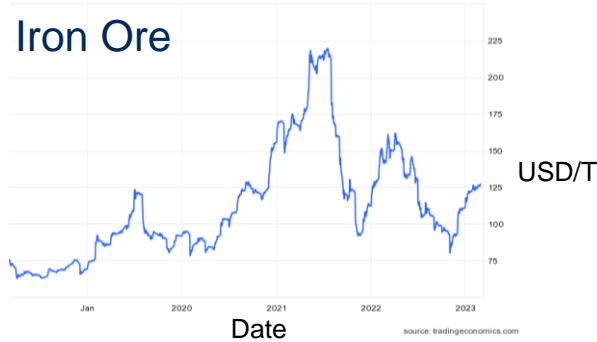
Materials

- Exotic materials
- Non-standard components
- Procurement Lead Times

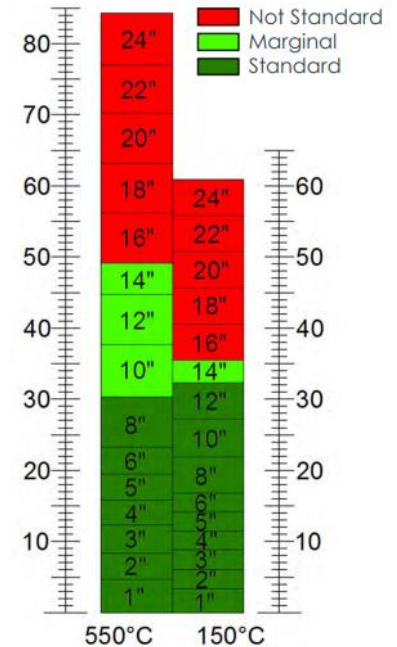
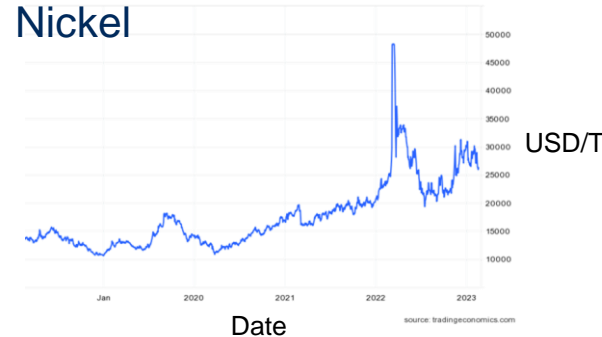


Grade	Ni (wt%)	Co (wt%)	Mo (wt%)
316L	11	0	2
617	52	9	12

Iron Ore



Nickel

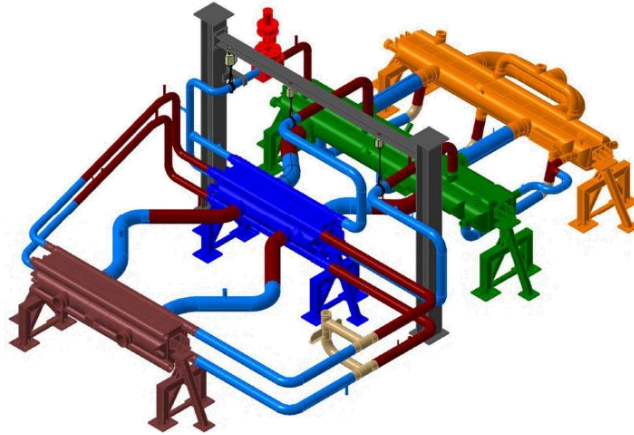


316 Pipe thickness vs. Std Pipe schedule (250 Bar pressure)

Challenges

Complexity

- Novel
- Engineering Development
- Reduced Agility



Solutions

Modularisation

- Smaller components
- Reduced Lead Times
- Efficient Engineering Design
- Improved Control
- Reduced Downtime



Path to Commercialisation



MAN Energy Solutions
Future in the making



STEP
DEMO



R&D activities on sCO₂ in Europe: Recuperators and coolers

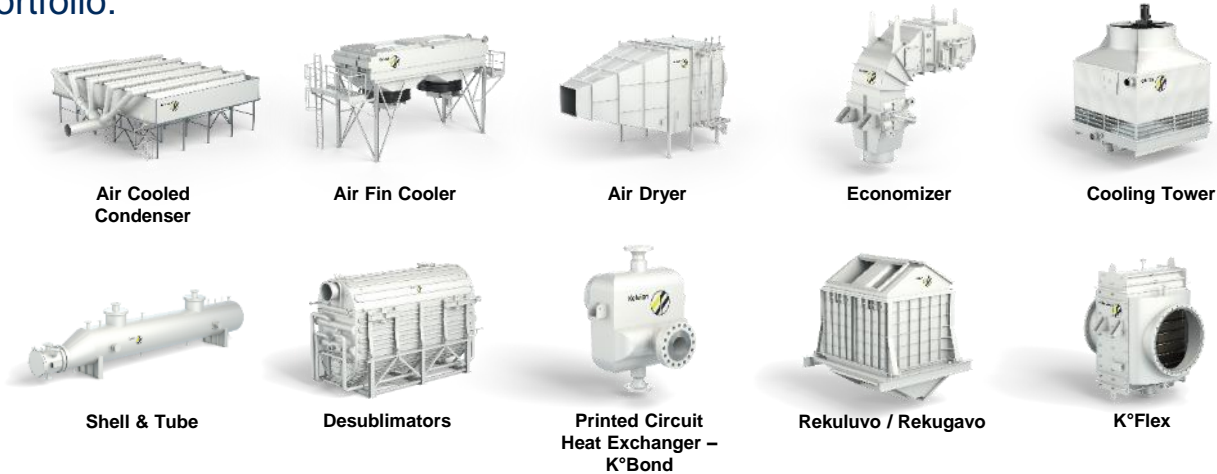
Improvement of dry air cooler for condensation of blended CO₂ using enhanced tubes

Summary

- Kelvion Thermal Solutions
- What is an Air Fin Cooler (AFC) ?
- Enhanced finned tubes
- Test tube section
- Prototype
- Full scale savings

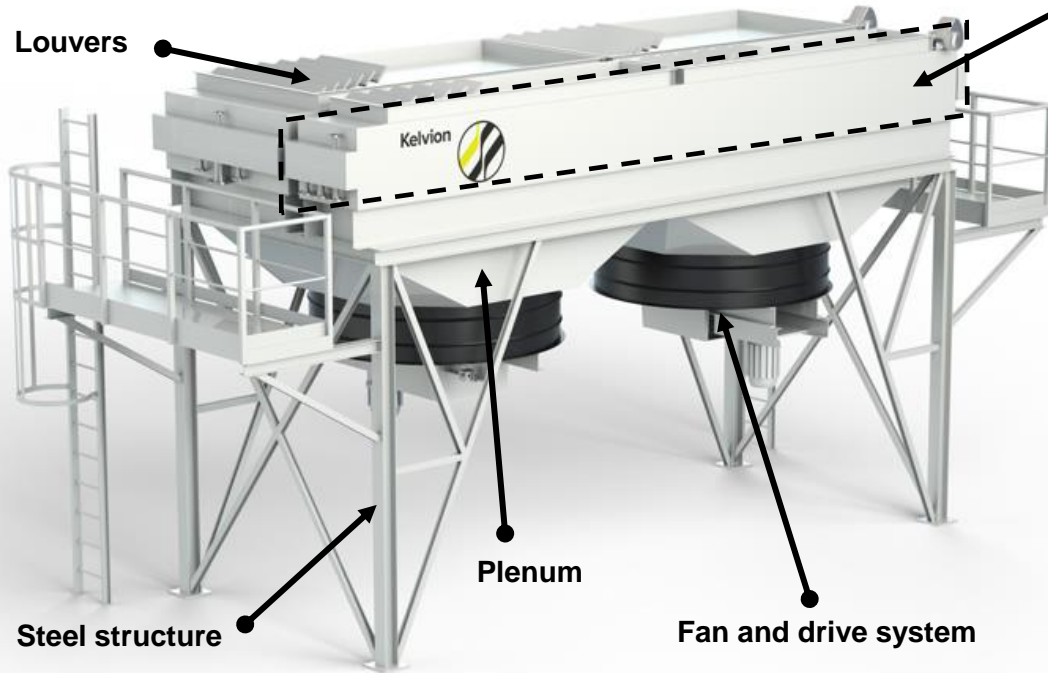
Kelvion Thermal Solutions

- Experts in heat exchange – Since 1920
- 1500 employees all over the world
- Five manufacturing sites based in US, China, France, Poland and Netherlands
- Large portfolio:

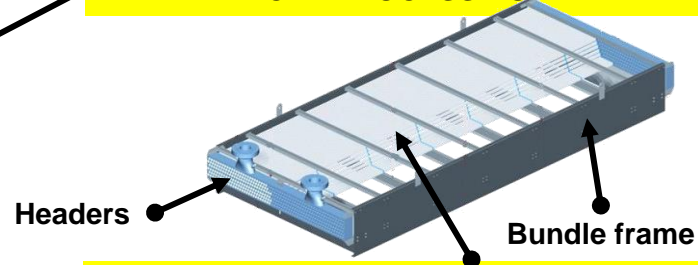


What is an Air Fin Cooler (AFC) ?

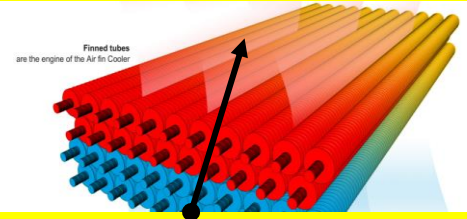
AFC ALU Forced draft (fan below bundle)



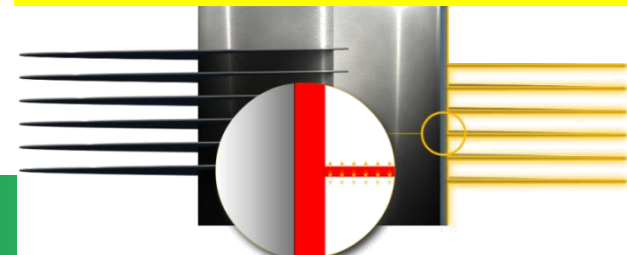
TYPICAL PROCESS BUNDLE



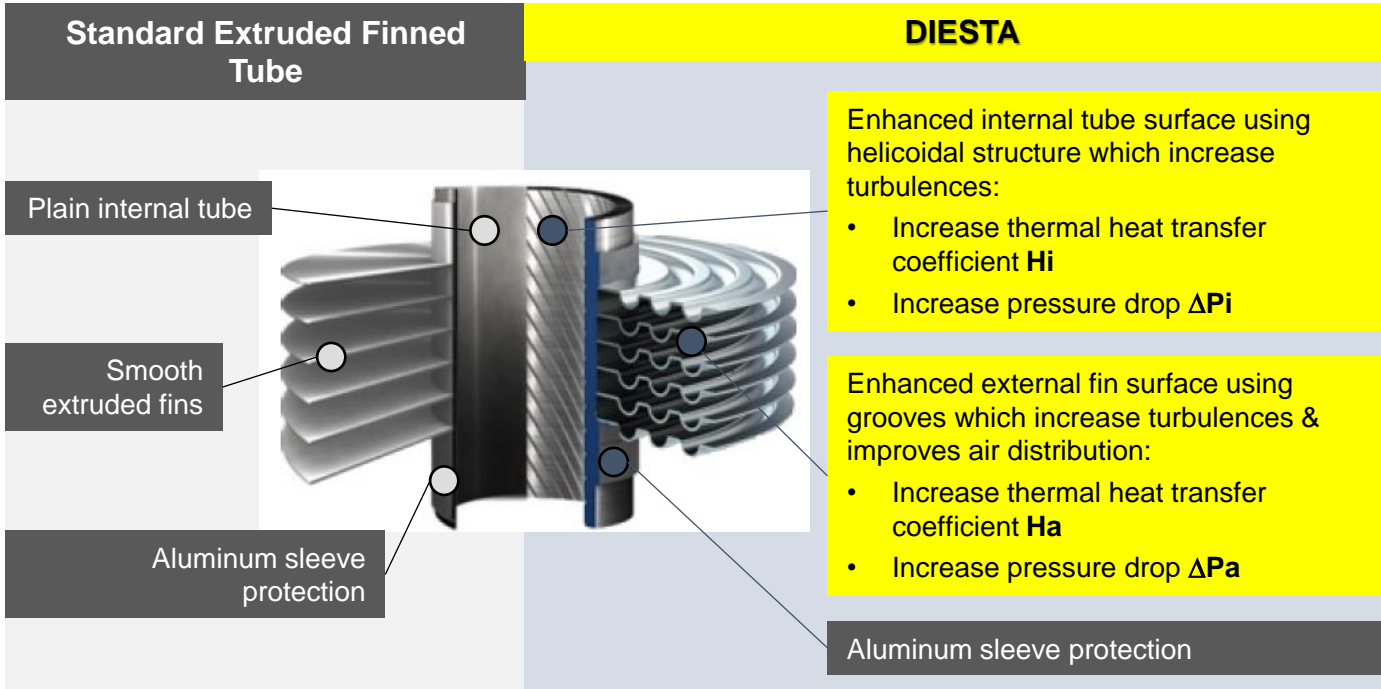
FINNED TUBES



TYPICAL FINNED TUBE

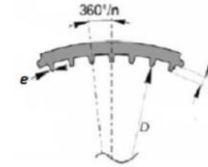
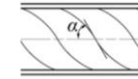


Enhanced finned tube



Helicoidal inner fins : challenge

Kelvion



- The inner fins geometry and performance depends on four parameters
 - Fin number n
 - Fin height h
 - Fin thickness e
 - Fin helix angle α
- In literature, some tests have been conducted with small diameter tubes (from 3 mm to 15 mm) and none with blended CO_2
- For full scale installation with high mass flow, such small diameters would create too much pressure drop. In this case, most economical solution for air cooled condenser is 1" tubes (25,4 mm)
- Efficiency of fins are directly linked to the tube diameter

↪ As part of SCARABEUS project, tests have been organised with 1" tubes with the support of Technische Universität Wien (TUW)



Test tube section : principle

- 3 different test section have been tested :
 - plain tube (no inner fins) for reference
 - tube with a dedicated geometry for CO₂ gas cooling
 - tube with a dedicated geometry for CO₂ condensation
- Tests have been conducted with pure CO₂ and a blended CO₂ (CO₂ + R1234ze)
- Tube have been instrumented with sensors in order to calculate the local heat transfer coefficients (and pressure drop)

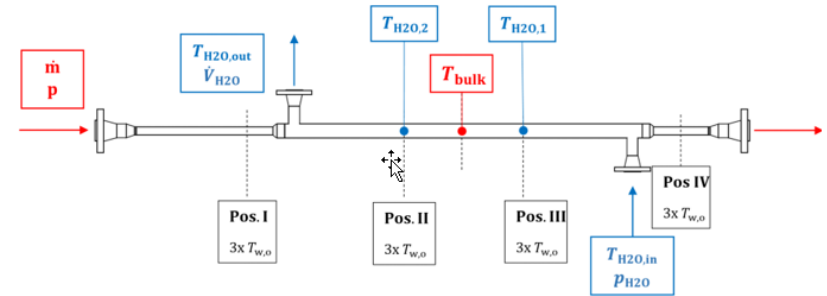


Figure 1: schematic of current test tube for heat transfer measurements when cooling and condensing; red...working fluid, blue...water, black...wall temperature.

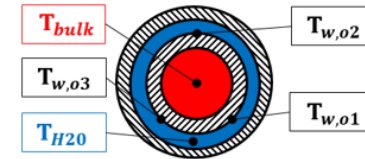


Figure 2: position of the temperature sensors at the cross section of the current test tube.

Test tube section : results

- For plain tube, the experimental HTC of the CO₂+R1234ze mixture fit very well with the ones calculated by Cavallini corrected by the Bell-Ghaly approach: most of the data points are within a range of ±10 %.
- For CO₂ condensation with inner fins, the improvement on HTC compared to plain tube can reach +40% for a pressure drop increase of 50 %.
- The improvement ratio is variable depending of the vapor content and the mass flux.

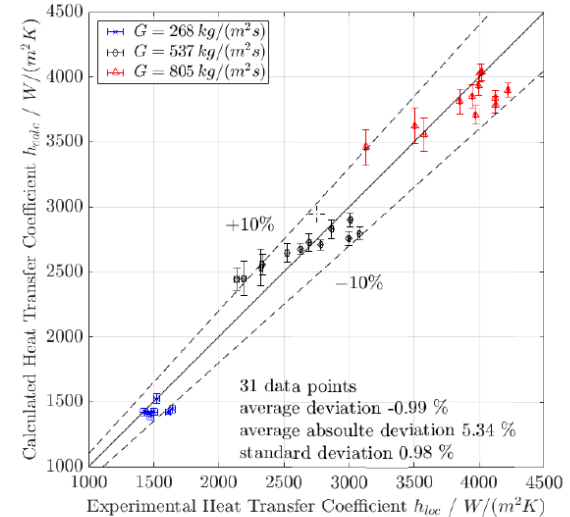
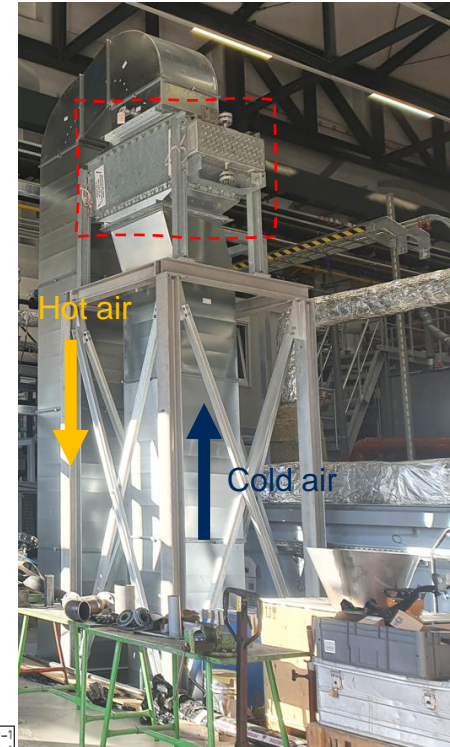
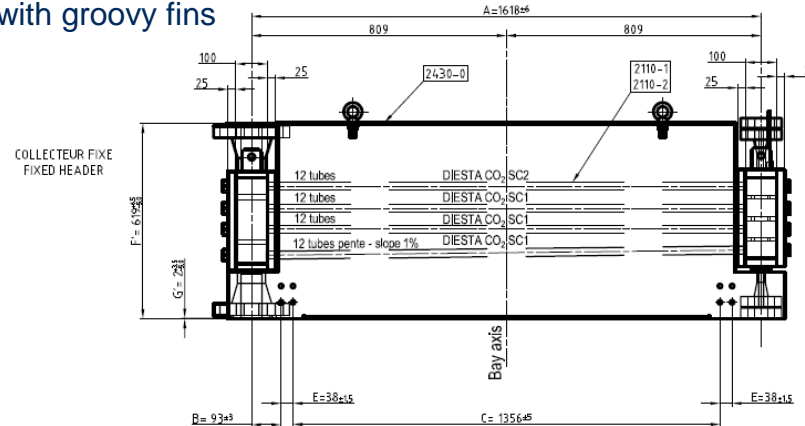


FIGURE 3: COMPARISON OF EXPERIMENTAL TO CALCULATED HEAT TRANSFER COEFFICIENTS OF THE MIXTURE CO₂+R1234ze(E).

Prototype

- A prototype has been manufactured and will be tested in TUW in 2023
- Design : 4 rows / 4 passes
- Operating conditions : 87 bar g / 152 °C with blended CO₂
- First passe with dedicated inner fins for gas cooling (DIESTA CO₂ SC2)
- Others passes with dedicated inner fins for CO₂ and CO₂ blend condensation (DIESTA CO₂ SC1)
- Air side : enhancement with groovy fins



Full scale savings

	Standard ACC	Kelvion technology	Unit	Savings
Total Duty	235	235	MW	-
Ambient air	36	36	°C	-
Number of fan	3	3	per bay	-
Fan diameter	17	17	ft	-
Tube length	18.3	18.3	m	-
Number of tube per bay	413	413	-	-
Number of bay	19	16	-	-15.8%
Total price including 33% VSDS	6,745,000	5,460,000	€	-23.5%
Price per bay	355,000	341,250	€	-3.9%
Total weight	1302	1080	Tons	-20.5%
Fan total consumption	2451	2304	kW	-6%

Conclusion : The combination of new inner fins and groovy fins on airside allows to reduce the plot plan, the CAPEX, the OPEX and the carbon footprint.

Thank you for your attention