



## **EXPERIMENTAL INVESTIGATION RESULTS OF A HYBRID CERAMIC AND ACTIVELY COOLED BALL BEARING FOR GAS TURBINES**

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# HYBRID CERAMIC AND ACTIVELY COOLED BALL BEARING FOR GAS TURBINES

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# Motivation & Goal

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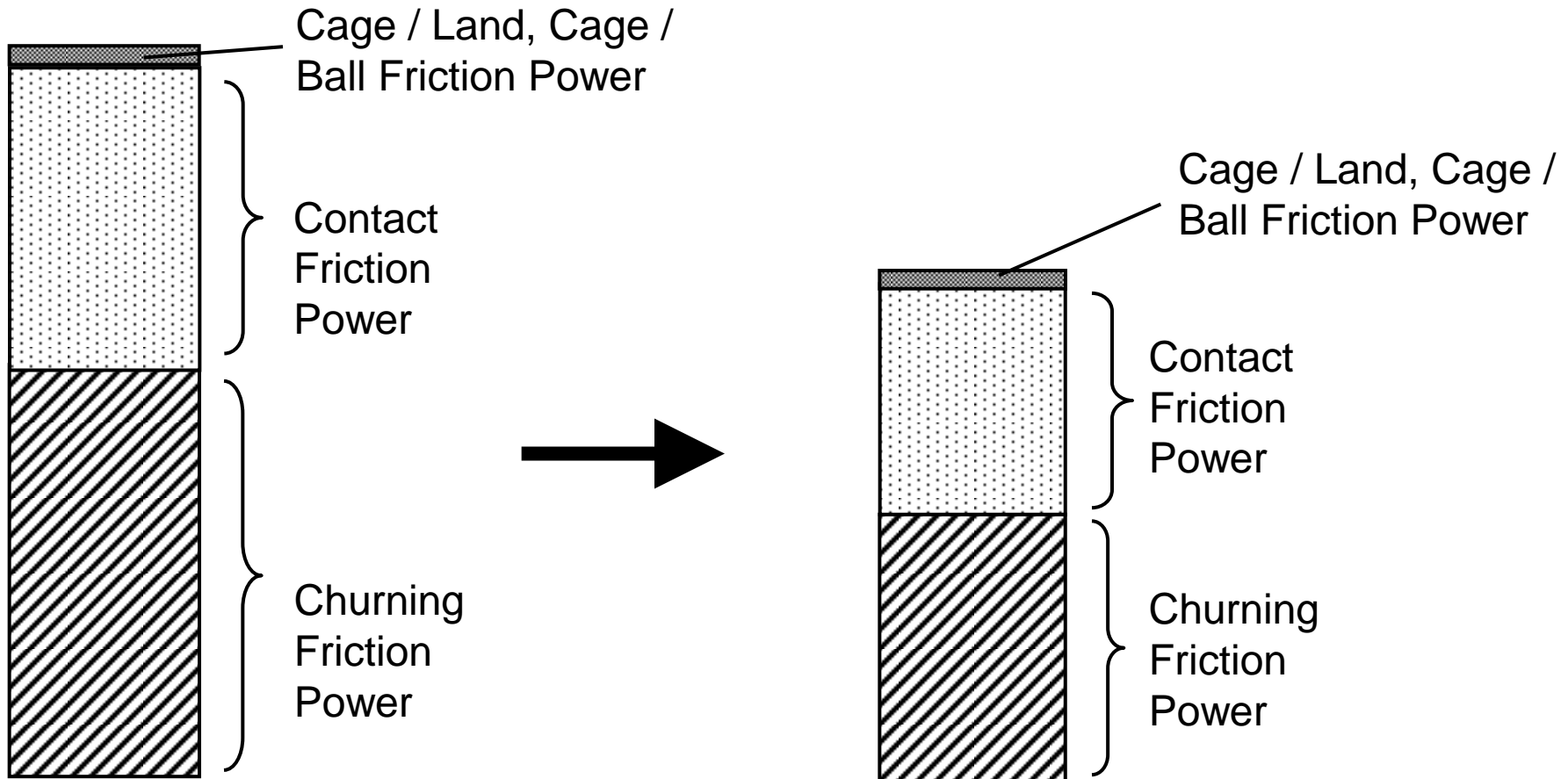
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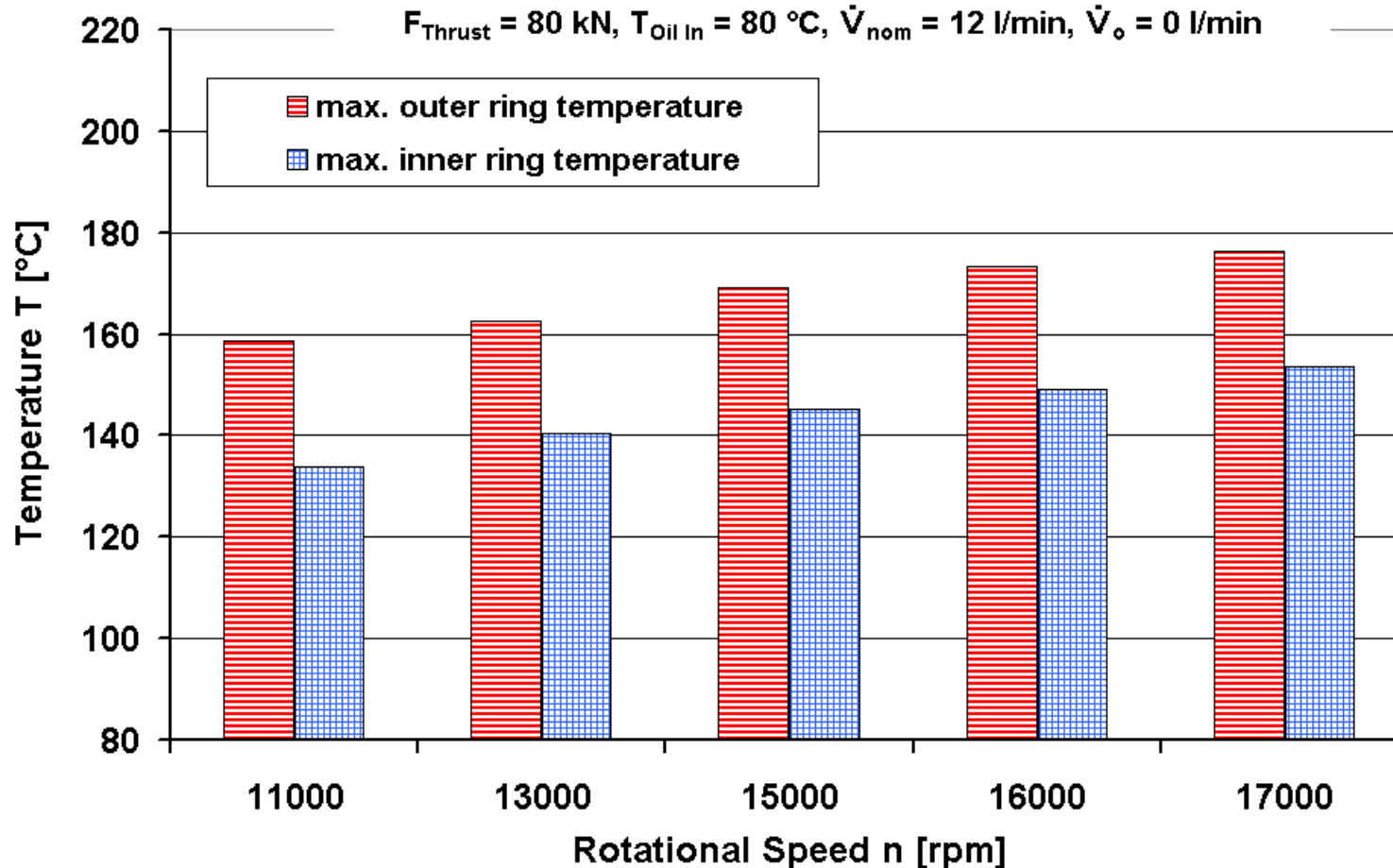
# Motivation

## Ball Bearing Friction Power



**Goal: Reduction of bearing power loss and thermal stressing.**

# Motivation

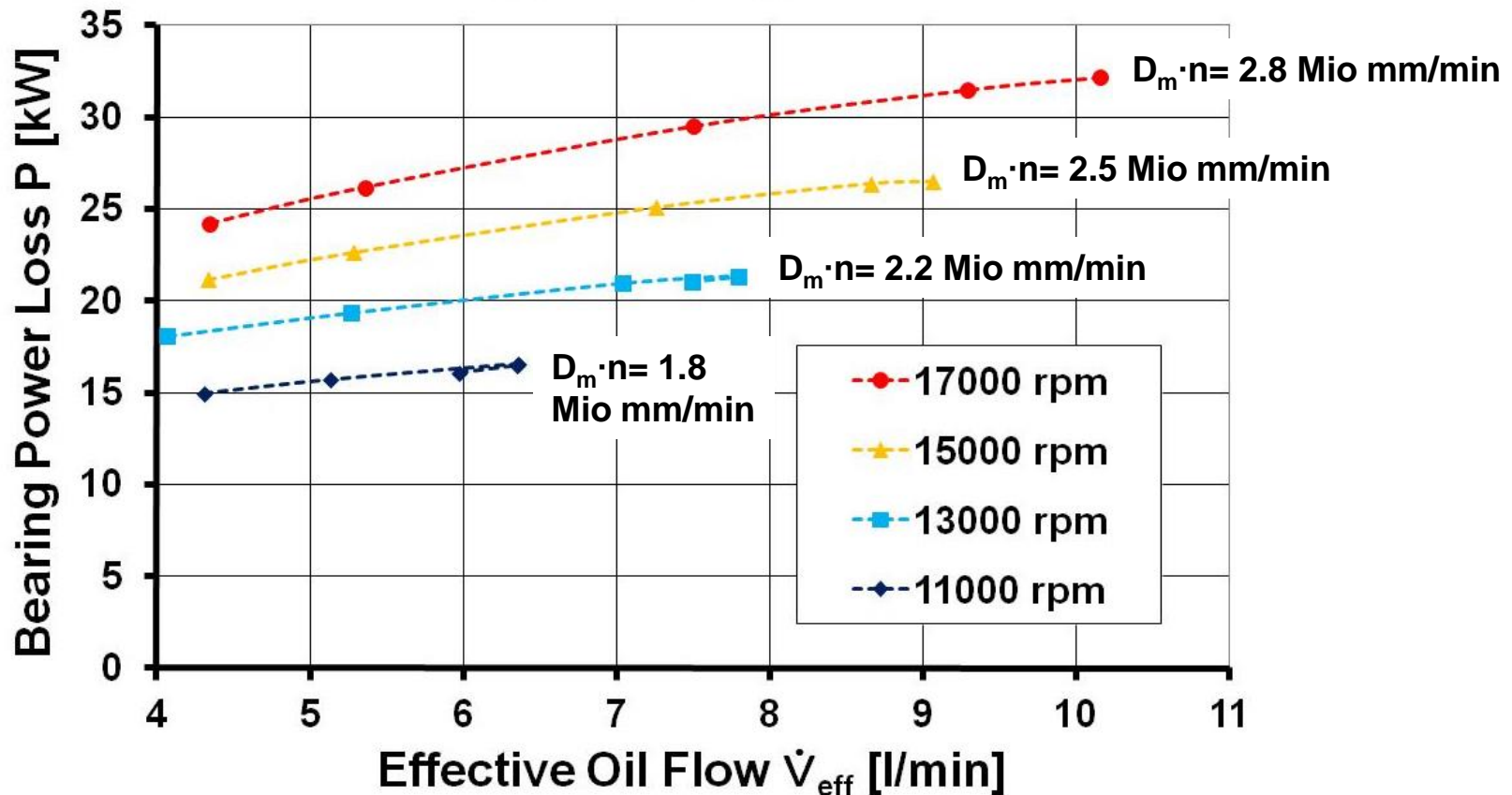


**For under-race lubricated bearings the outer ring is the temperature-critical component.**

# Motivation

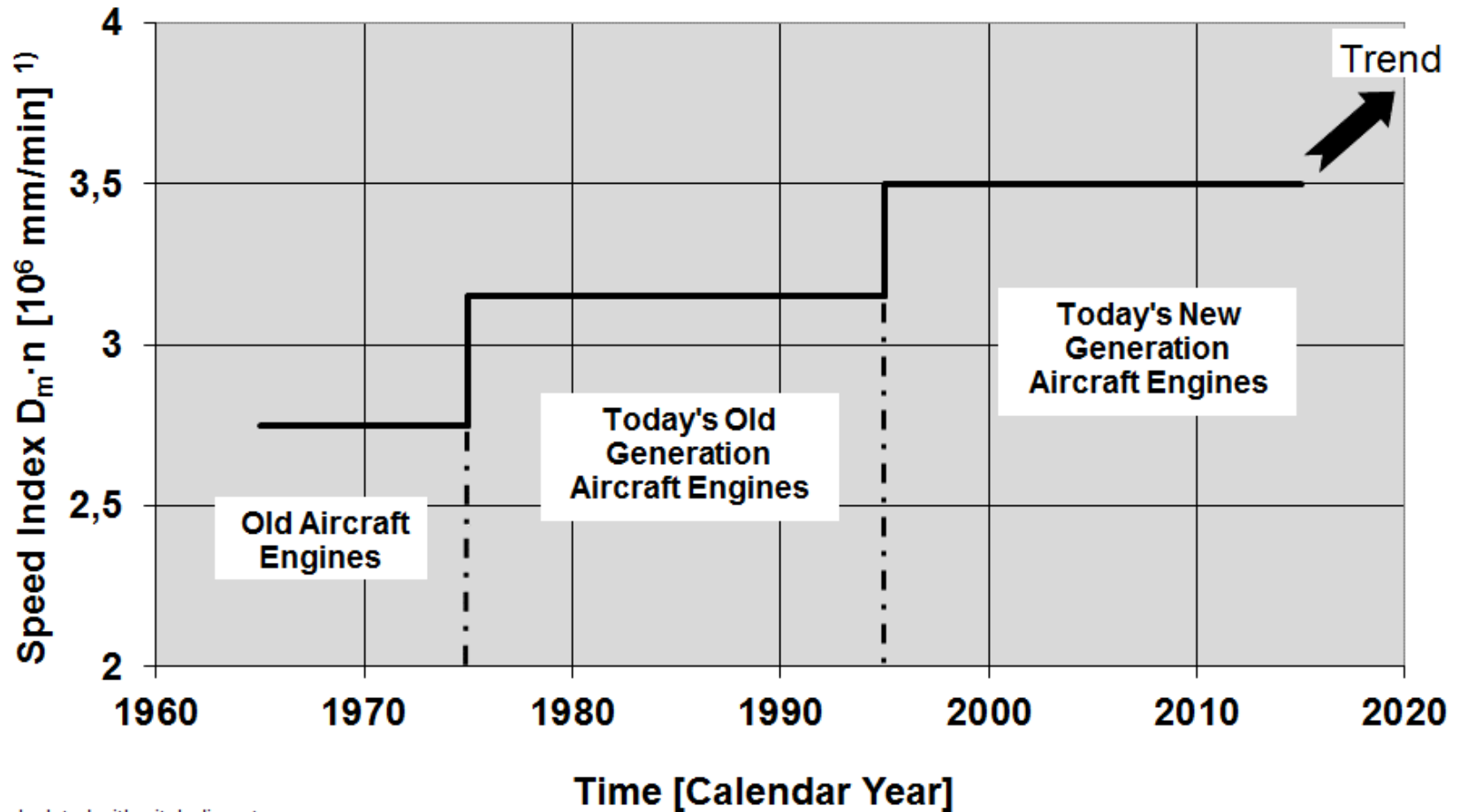
## Influence of Under - Race Oil Flow on Bearing Power Loss

$$F_{\text{Thrust}} = 80 \text{ kN}, T_{\text{Oil In}} = 80 \text{ }^{\circ}\text{C}$$



**A power loss reduction can be achieved by lower oil quantities  
...but we also need to control the raceway temperature**

# Motivation



1) calculated with pitch diameter

## Speed Index increases continuously for HP-Bearings

# Motivation & Goal

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## ECO-POLITICS

- The goals described by the European Commission and The Advisory Council for Aeronautics (ACARE) in "Flightpath 2050": reduction of 75% CO<sub>2</sub>, 90% NO<sub>x</sub>, and 65% noise compared to capabilities of typical new aircraft in the year 2000.

## END USER REQUIREMENTS

- End user require more efficient and performance-enhanced engine components. Approximately one third of an airline's total operating costs are contributed by kerosene costs.

## TECHNICAL REQUIREMENTS

- Rolling element bearings determine significantly the mechanical efficiency of an aircraft engine
- Today's state of the art main shaft bearing feature squeeze film damping in order to reduce vibrational loads



## Motivation & Goal

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### Goal:

### Increase of Reliability, Performance and Efficiency of Aircraft Engine Ball Bearings

Further additional reduction compared to an all-steel bearing:

- bearing power loss: 10 %
- required total oil flow: 15 %
- damping of rotor vibrations
- temperatures: 10 K
- increase of max. rotor speed by 20%

### Measures:

Use of:

- ceramic balls
- integrated squeeze film damper
- direct outer ring cooling concept
- plasma nitrided raceways



# Test Bearing and Rig Test Head Design, Test Conditions

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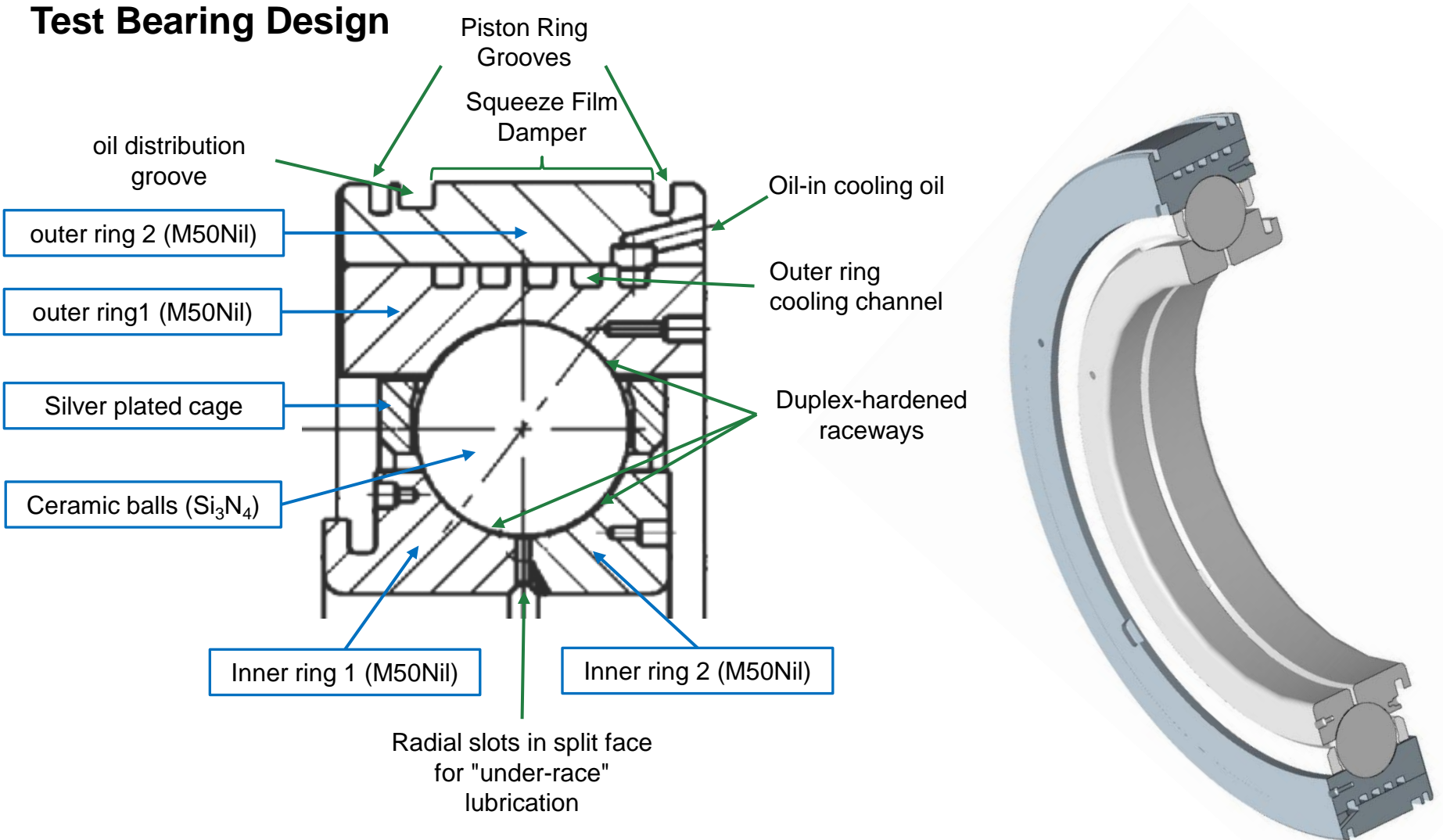
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# Test Bearing and Rig Test Head Design, Test Conditions

## Test Bearing Design

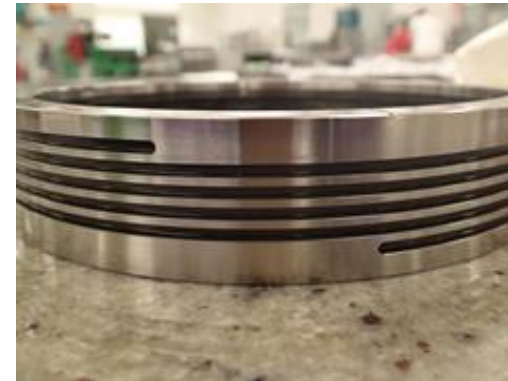


# Test Bearing and Rig Test Head Design, Test Conditions

## Bearing Components prior to Rig Test



outward outer ring featuring piston ring grooves for squeeze film damping



inward outer ring featuring helical cooling channel



loaded inner ring with radial oil slots in the split face

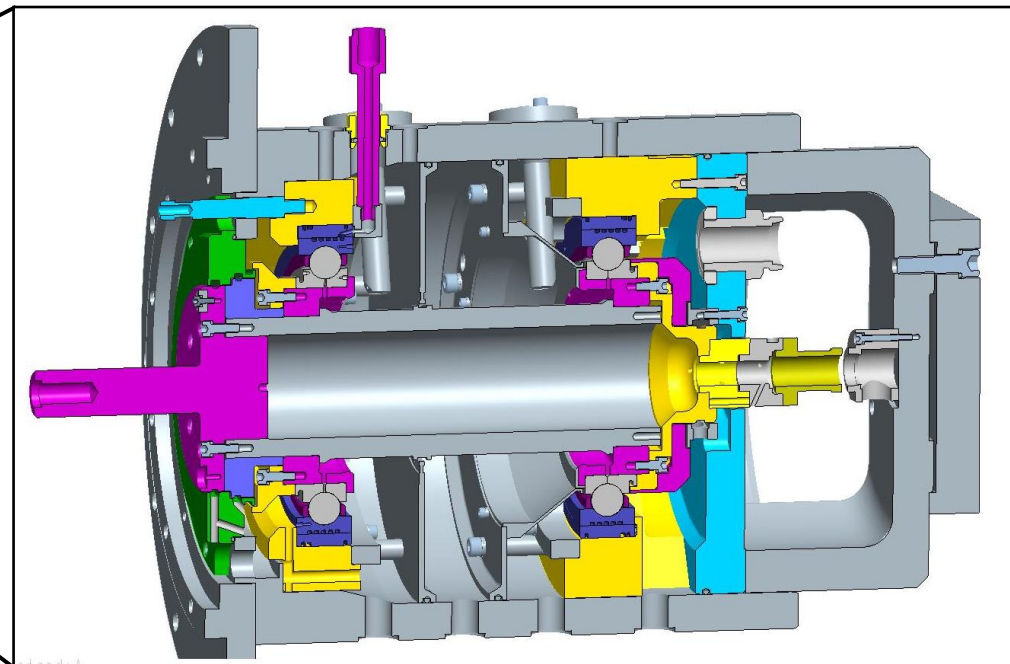
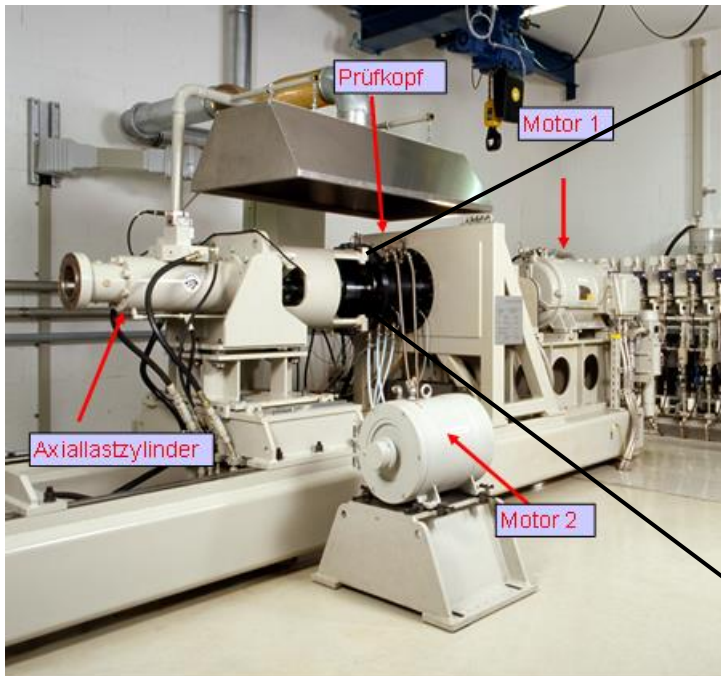


cage/ball assembly

# Test Bearing and Rig Test Head Design, Test Conditions

## Test Rig: AN62

- Location: Schweinfurt, Germany
- Speed Capability: depending on gearbox installed; w/ current gearbox up to 26000 rpm
- Motor Power: 120 kW (161 hp)
- Axial and radial loads up to 200 kN (45,000 lbf), misalignment testing
- capability for tests with co- and counter-rotating bearings (intershaft bearings)
- three independent oil systems
- sensor technology: static, telemetry, vibrations, piezo, strain gages, chip detectors, cage speed, etc.





## Test Bearing and Rig Test Head Design, Test Conditions

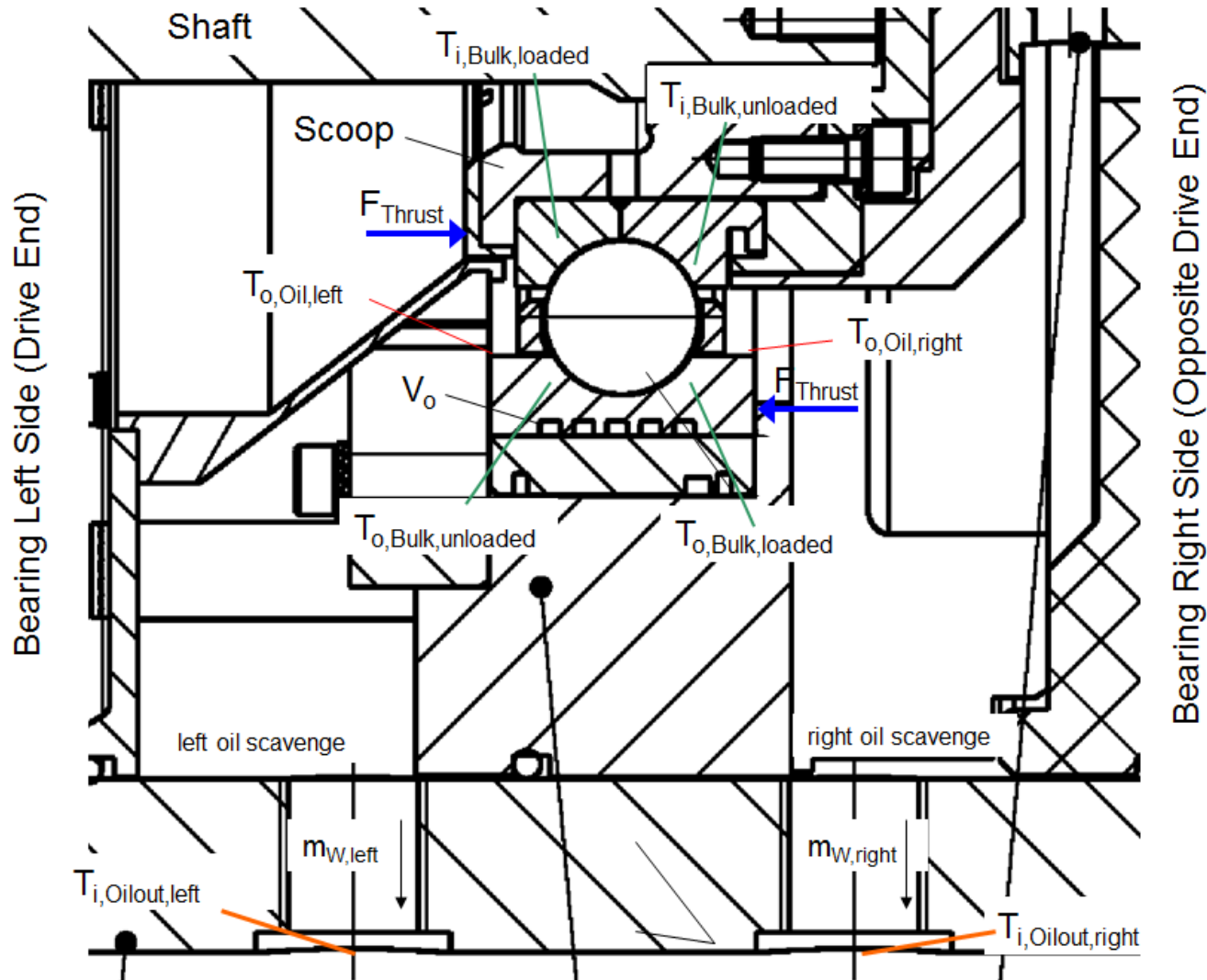
### Test Conditions:

- Rotational Speed: 14000 - 24000 rpm ( $D_m \cdot n = 2,35$  to 4 Mio mm/min)
- Axial Load: 26,7 - 80 kN ( $p_0 = 1540$  to 2440 MPa, [224 to 354 ksi])
- Oil In Temperature: 80°C and 110°C (176 and 230 °F)
- Under-race Oil Flow: 5, 6, 8, 10, 12 (14, 15) l/min (1.3 to 4 gallons/min)
- Outer Ring Channel Oil Flow: 0, 1, 2, 3, 4, 6, 8, 10 l/min (up to 0.8 gallons/min)
- Engine Oil per MIL-PRF 23699

### Measured Variables:

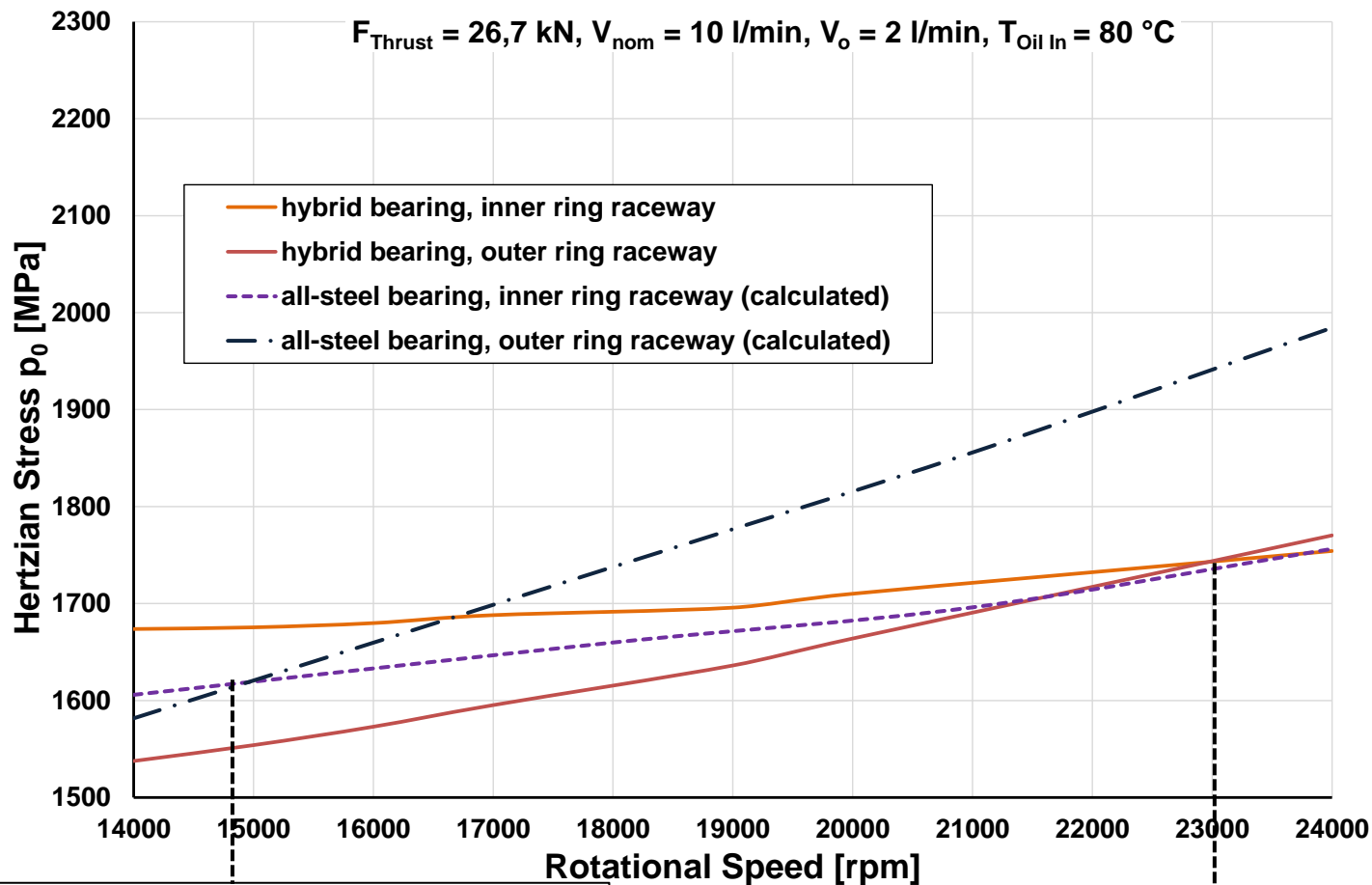
- Outer and Inner Ring Temperatures
- Bearing Power Loss
- Oil Flow Qty, Oil Pressure, Oil Temperatures
- Vibrational Accelartion
- Axial Load, Shaft Rotational Speed

# Test Bearing and Rig Test Head Design, Test Conditions



# Test Bearing and Rig Test Head Design, Test Conditions

## Hertzian Stress



identical Hertzian stresses for outer and inner race of steel brg

identical Hertzian stresses for outer and inner race of hybrid brg



# Experimental Investigation Results: Oil Flow

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# Experimental Investigation Results

## Pictures of rig tested hybrid bearing



loaded inner ring half



bearing with one inner ring half removed, showing the ceramic balls and the cage



cage/ball assembly



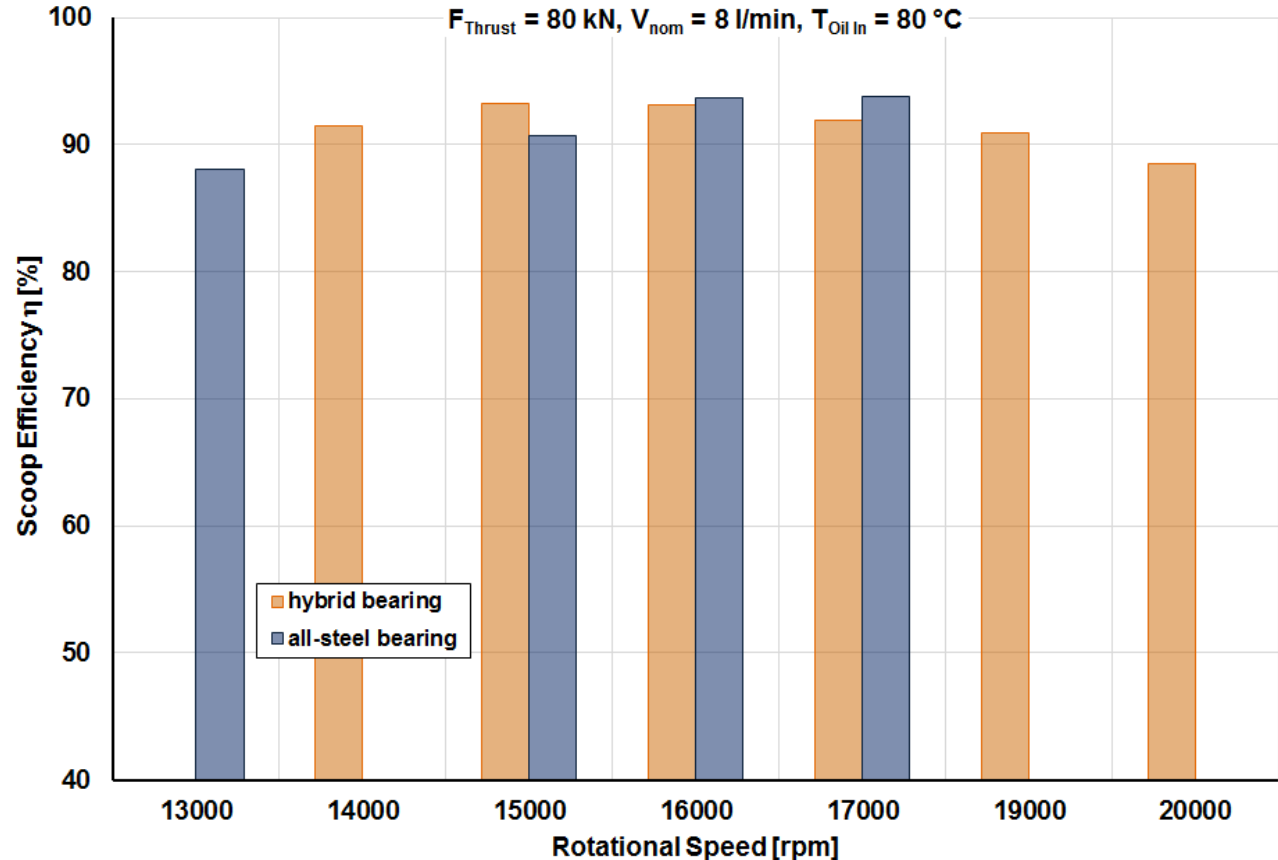
outer ring



bearing side view

# Experimental Investigation Results: Oil Flow

$$\eta = \frac{m_{W,left} + m_{W,right}}{m_{nom}}$$



**Scoop Efficiency very similar between all-steel and hybrid bearing  
 → enables direct comparison of steel and hybrid bearing**

# Experimental Investigation Results: Temperatures

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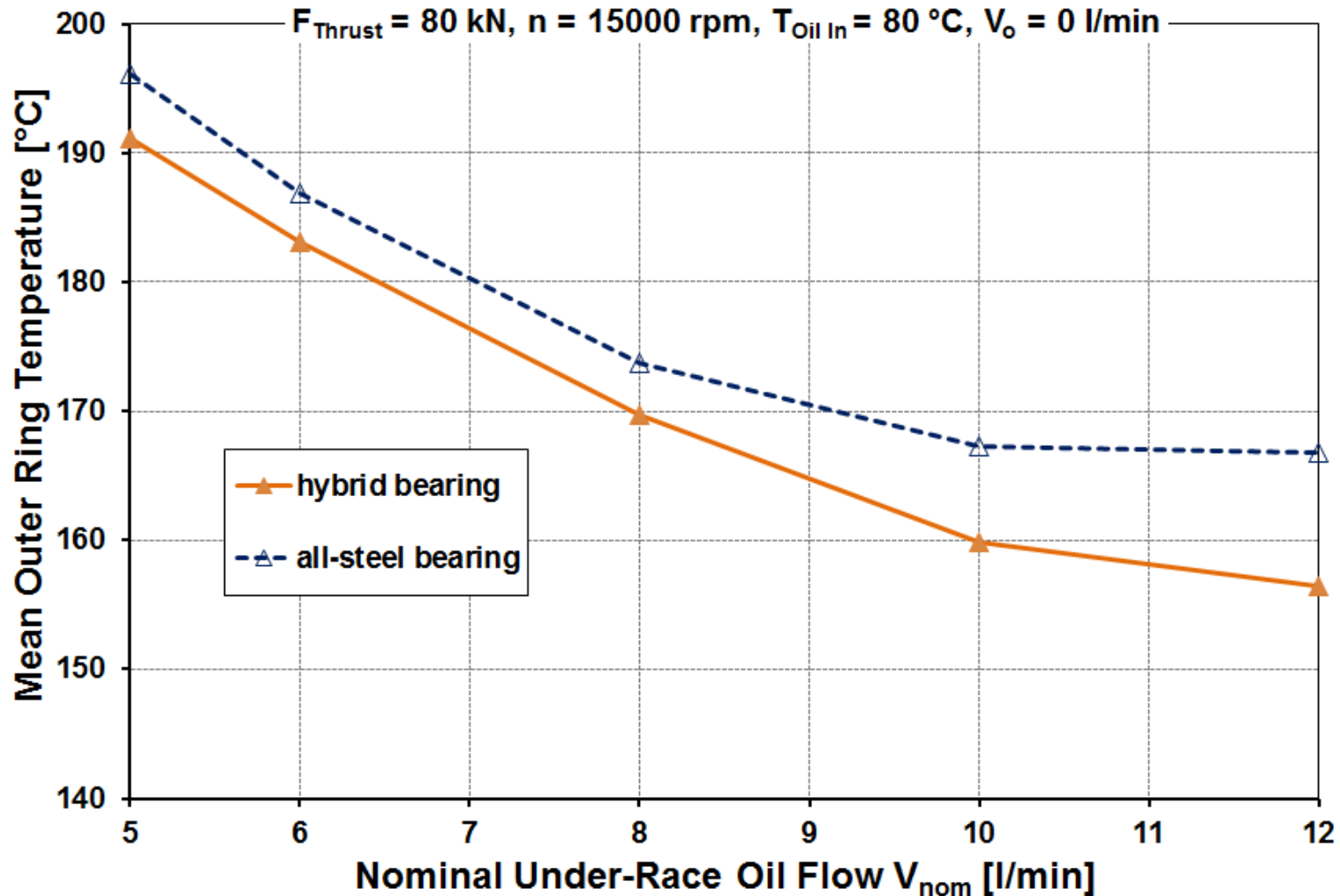
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Experimental Investigation Results: Bearing Power Loss & Heat to Oil (HTO)

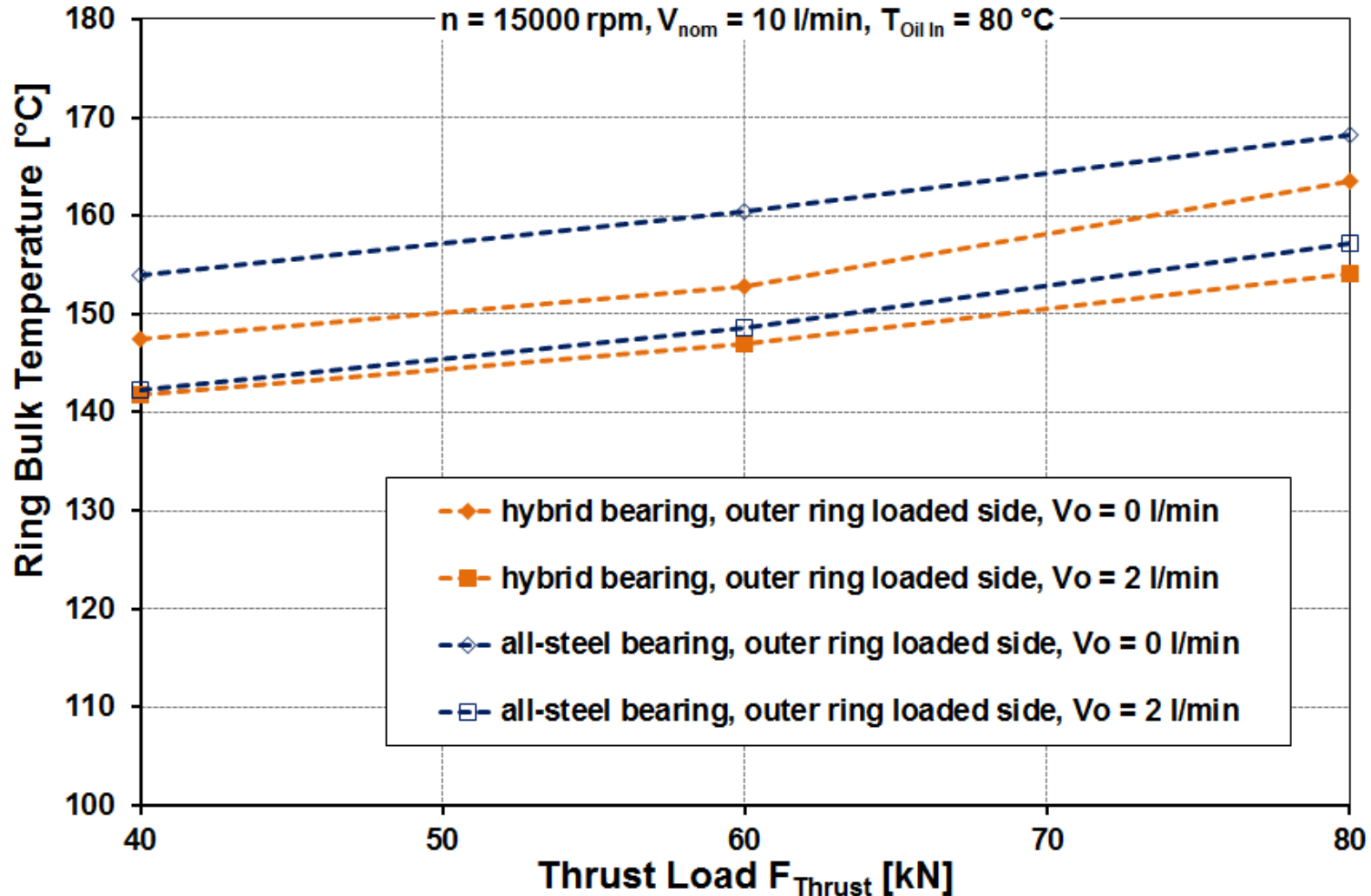
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Summary and Conclusion

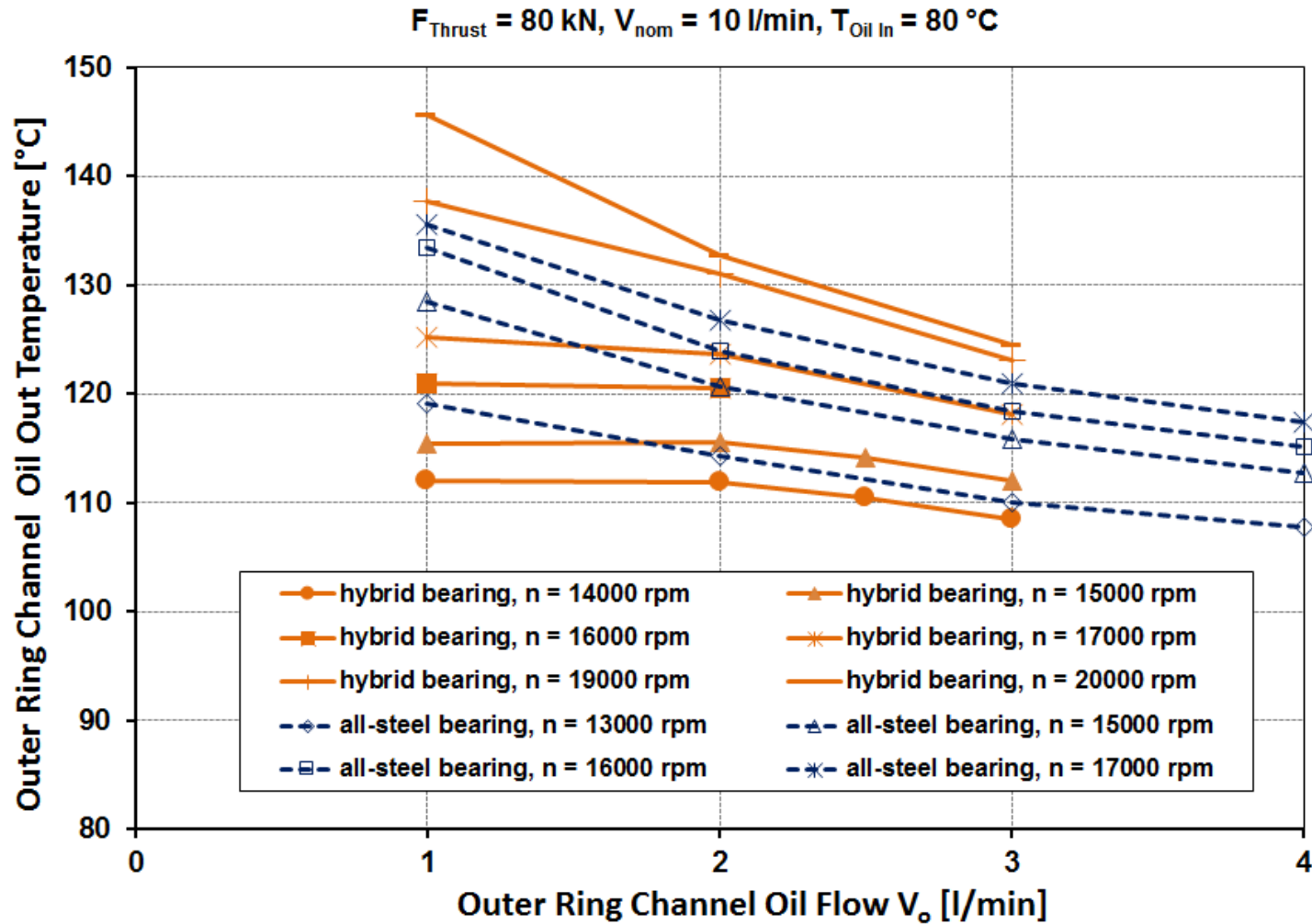
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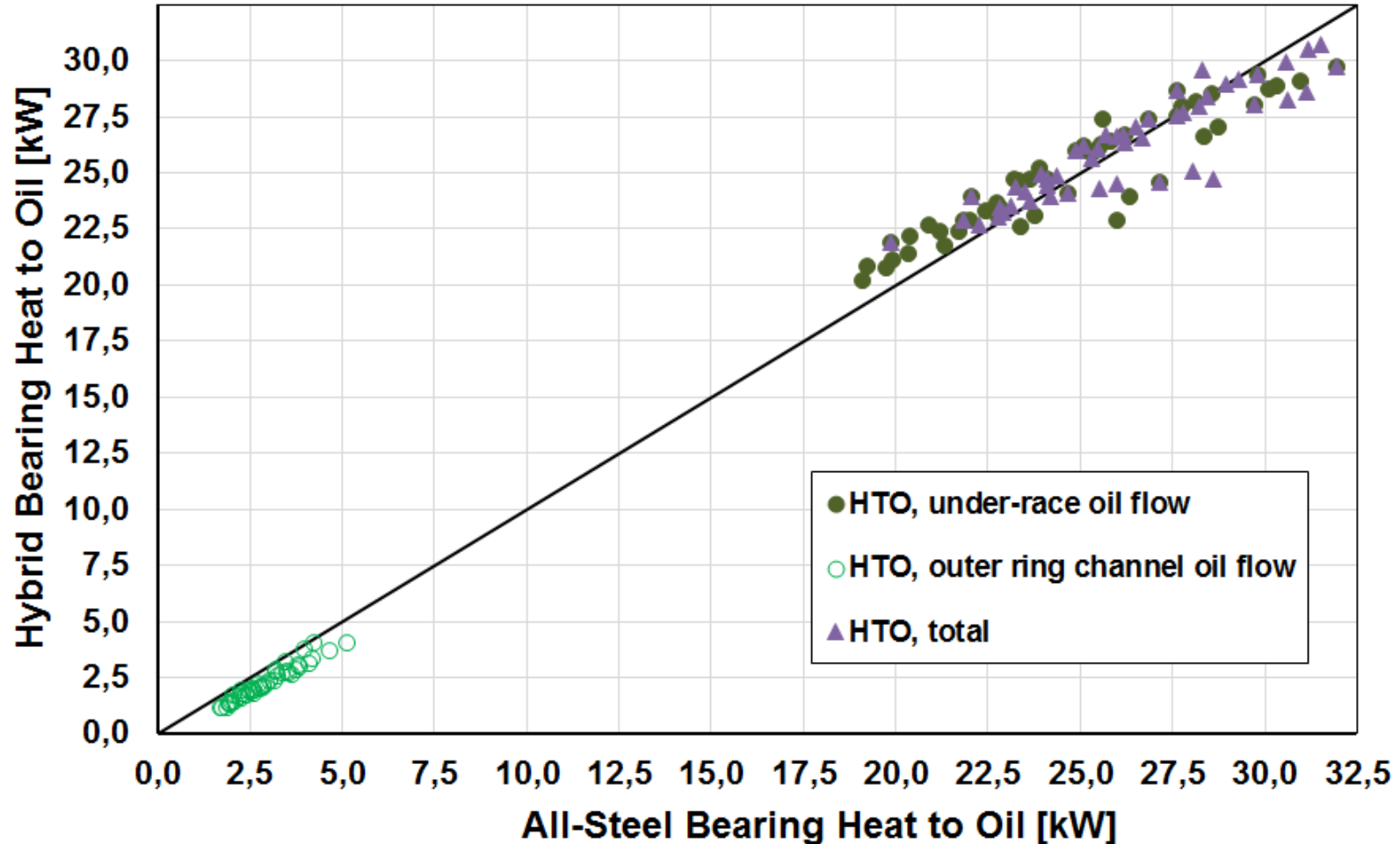
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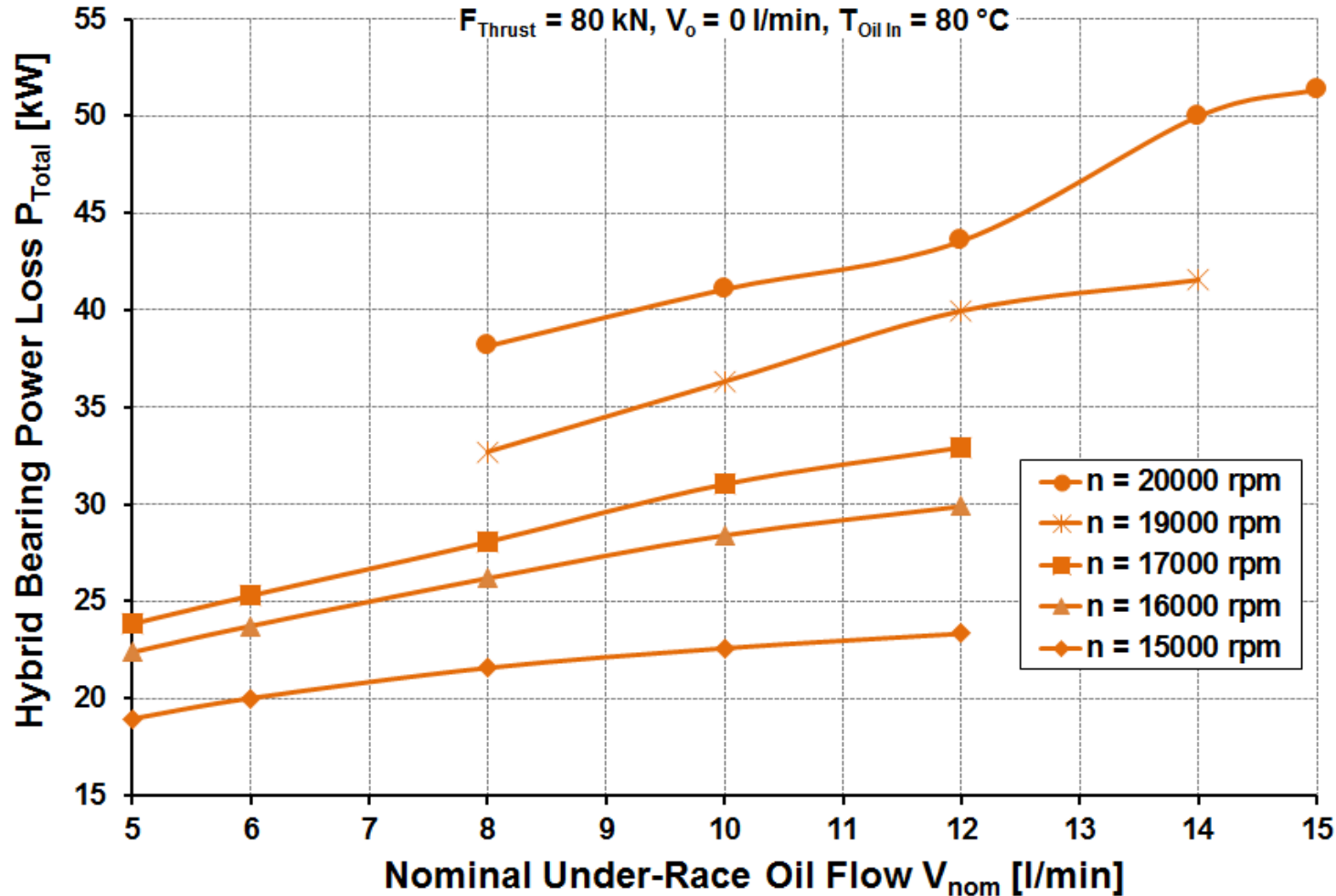


# Experimental Investigation Results: Bearing Power Loss & Heat to Oil (HTO)

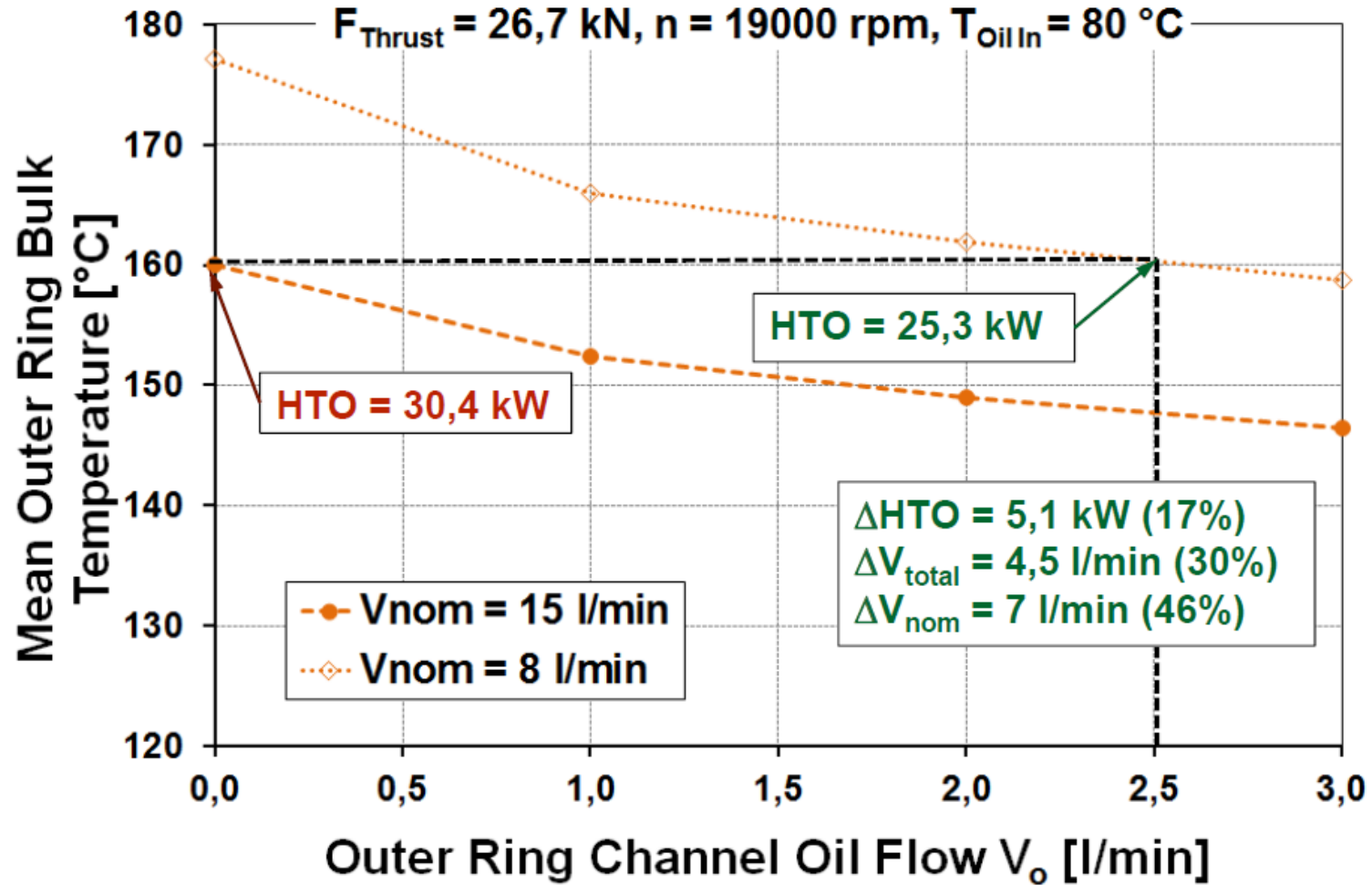
$$HTO = m_w \cdot c_p \cdot (T_{Oilout} - T_{OilIn})$$



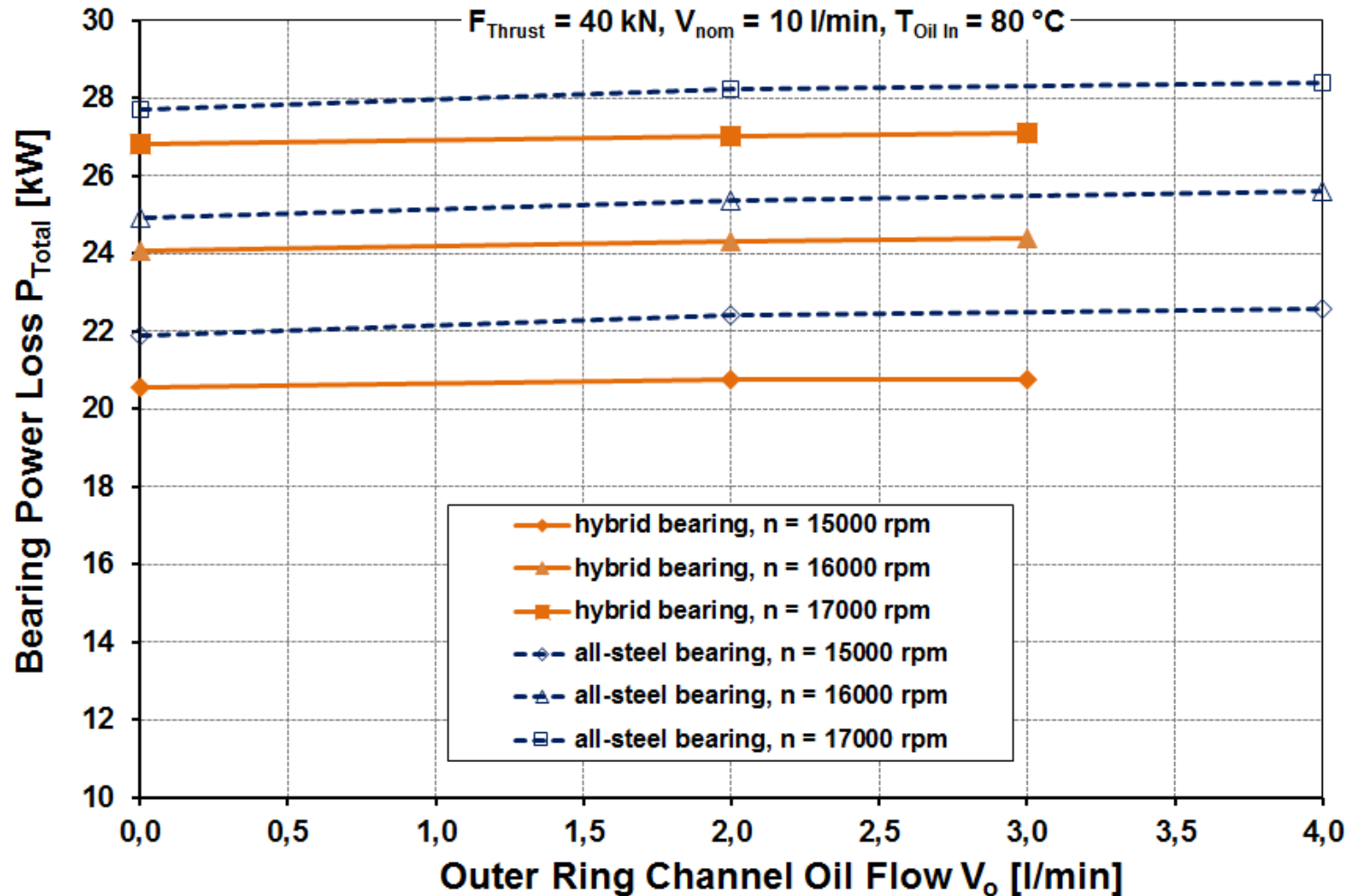
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# High Speed Capability

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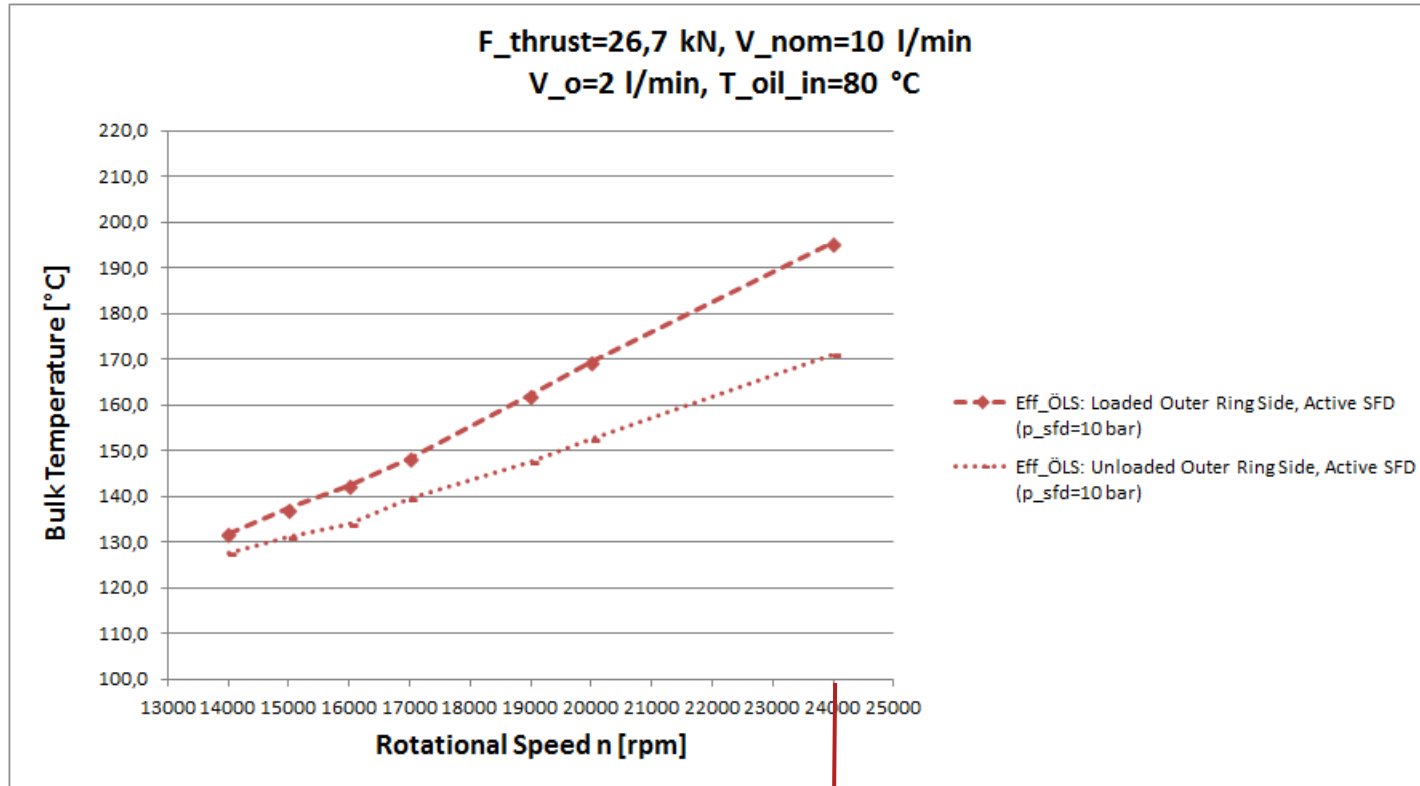
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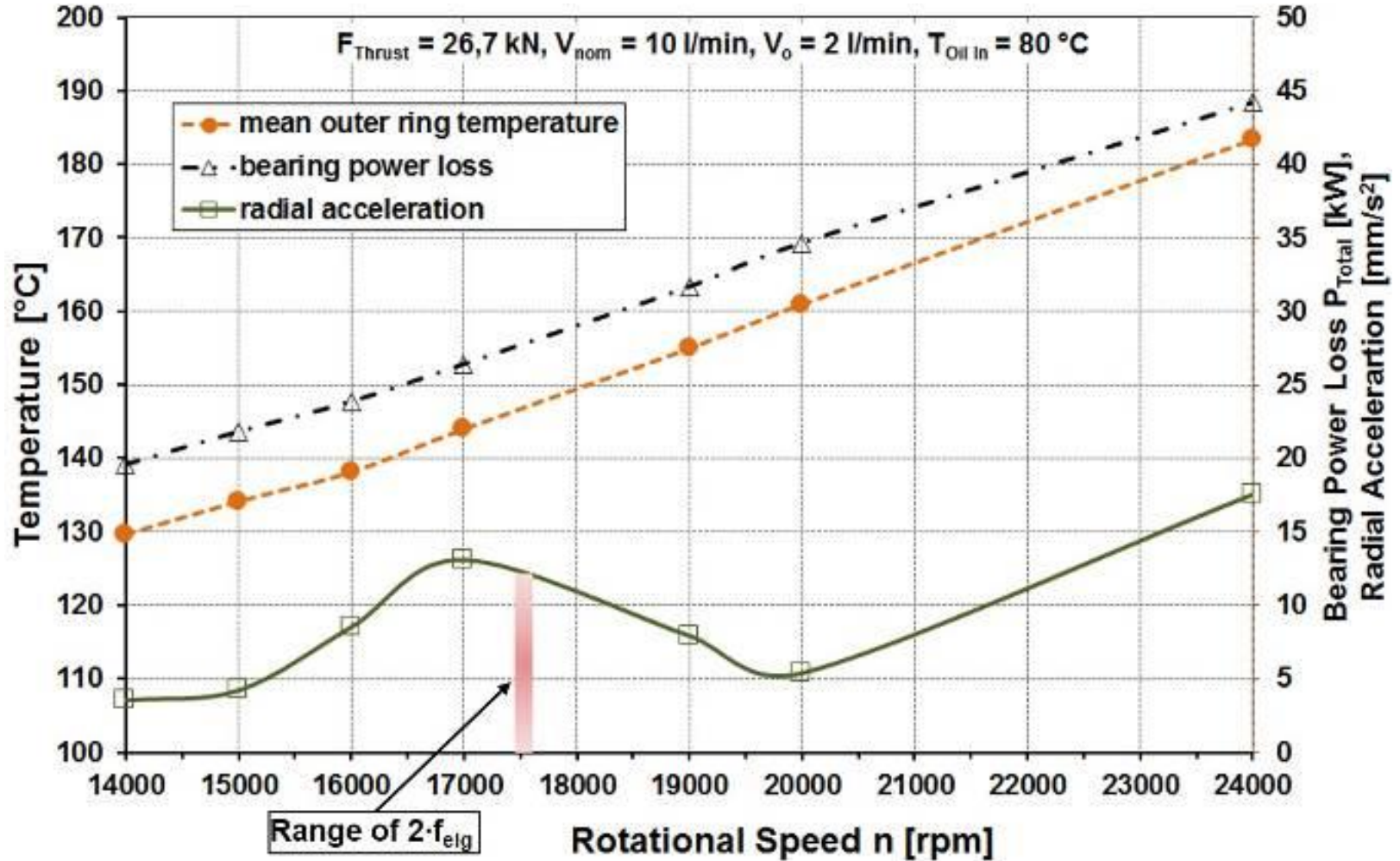
# High Speed Capability



$D_m \cdot n = 4,02 \text{ Mio mm/min}$

**Speed Index > 4 Mio mm/min at T<sub>OR</sub> < 200°C achieved by selective adjustment of under-race and outer ring channel oil flow quantity**

# High Speed Capability



# Conclusion & Outlook

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## Conclusion & Outlook

### Specific Benefits:

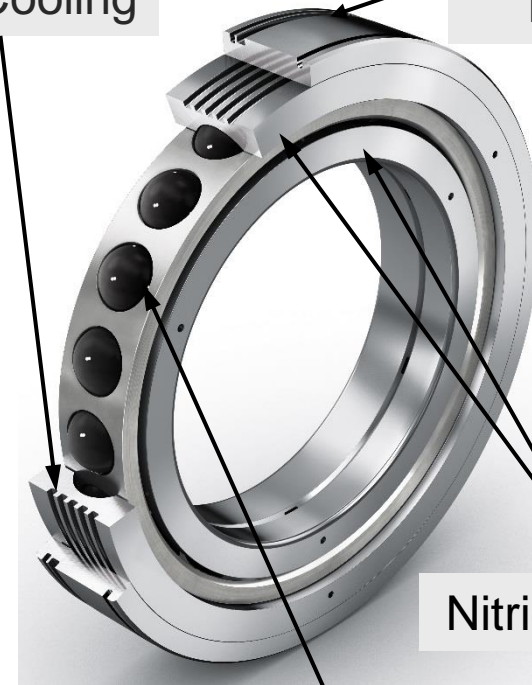
- Oil Flow Savings up to 50 %
- Power Loss Reduction up to 25 %
- up to 25 K lower temperatures
- High speed capability above  $4 \cdot 10^6$  mm/min

### Overall Benefits

- Increase in mechanical efficiency (bearing & engine)
- Reduction of weight (smaller oil pump etc.)
- Reduction of engine fuel consumption
- Reduction of engine emissions
- Improvement in material fatigue strength (from lower brg temperature)
- Increase of reliability
- Reduction of total cost

Direct Outer  
Ring Cooling

Squeeze Film  
Damping



Nitrided Races

Ceramic Balls

## Conclusion & Outlook

### Fuel Consumption Benefit by using Direct Outer Ring Cooled Hybrid Ball Bearing

#### Calculation Example:

- Bearing Power Loss Reduction: 4 kW per bearing
- #3 ball bearing (HP shaft) with DORC
- 4 kW saving per gas turbine
- Heat Value (Jet A1): 42500 kJ/kg
- Overall Engine Efficiency: 38 %
- Gas Turbine fleet: approx. 5000 engines in service



Source: GE Aviation

→ Kerosene savings per engine: 7800 kg/a (CO<sub>2</sub> savings: 25 t/a)

→ Kerosene savings for fleet: 39000 t/a (CO<sub>2</sub> savings: 123000 t/a)

→ USD savings\* for **fleet: 16 Mio USD/a** (45000 USD/d)

→ USD savings\*\* for **fleet: 31 Mio USD/a** (84000 USD/d)

\* US\$/bbl = 53; \*\* US\$/bbl = 100;

# HYBRID CERAMIC AND ACTIVELY COOLED BALL BEARING FOR GAS TURBINES

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**Thank you for  
your attention!**